

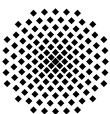
Freudenstadt, March 2006

***A Phenomenological Model Concept
for the Numerical Simulation of
Two-Phase Two-Component Processes
in Cohesive Soils***

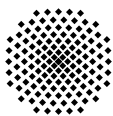
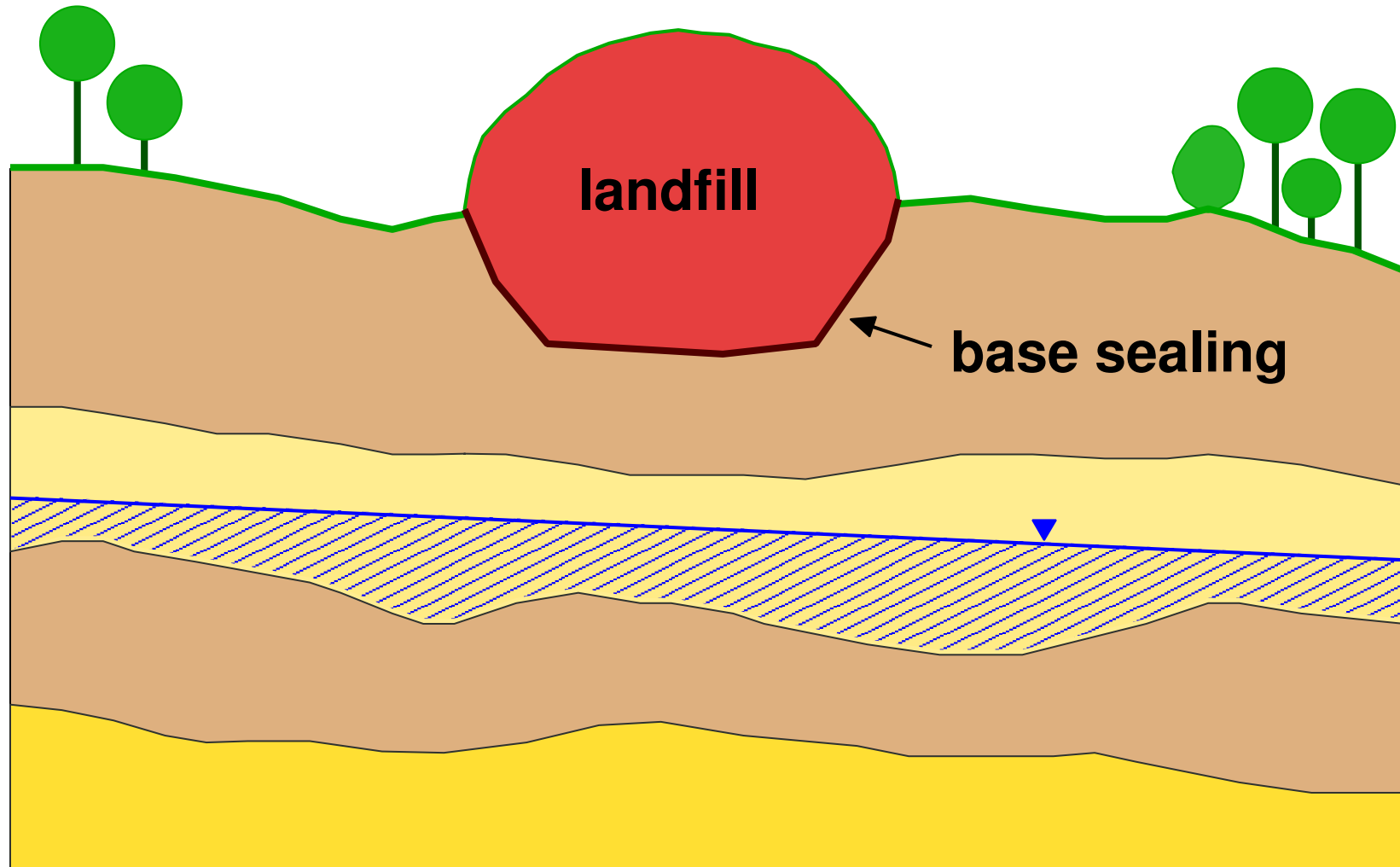
Sandra Freiboth, Holger Class, Rainer Helmig

Lehrstuhl für Hydromechanik und Hydrosystemmodellierung

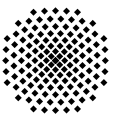
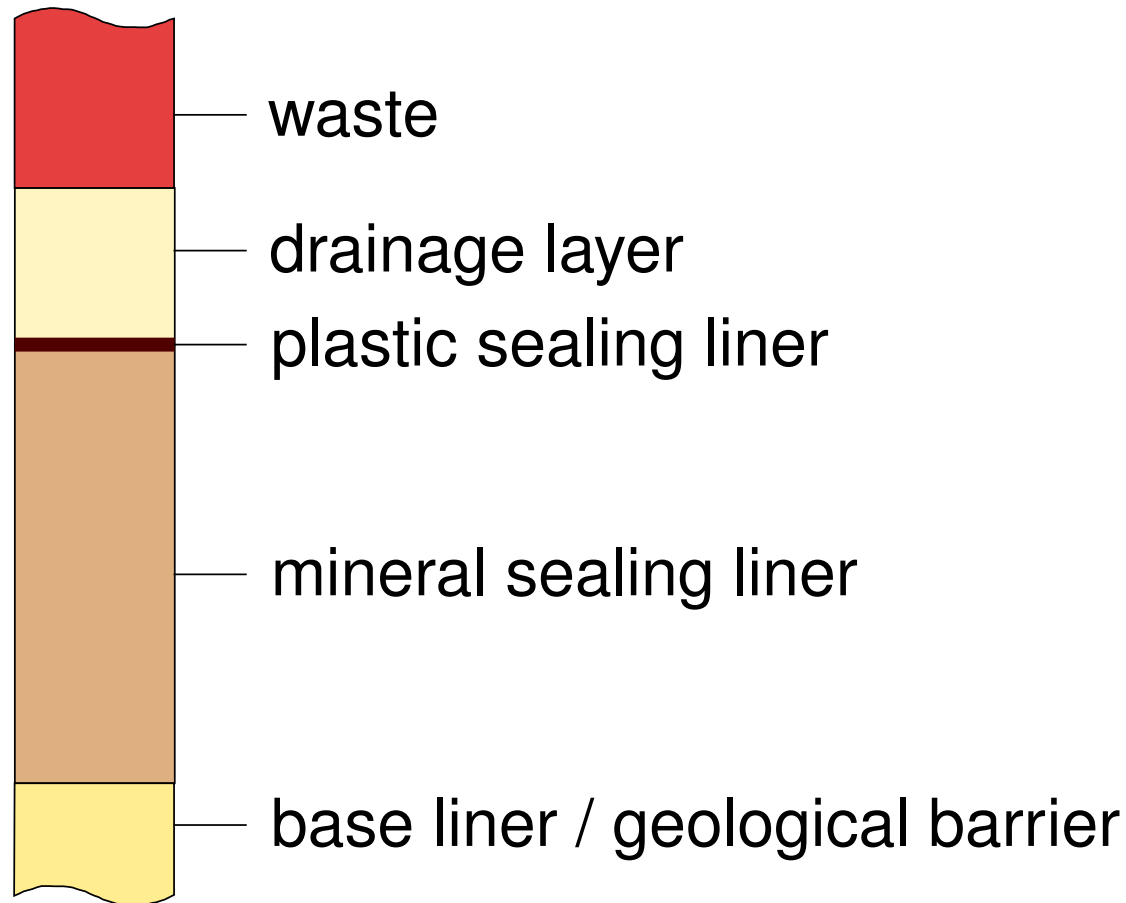
Institut für Wasserbau, Universität Stuttgart



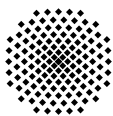
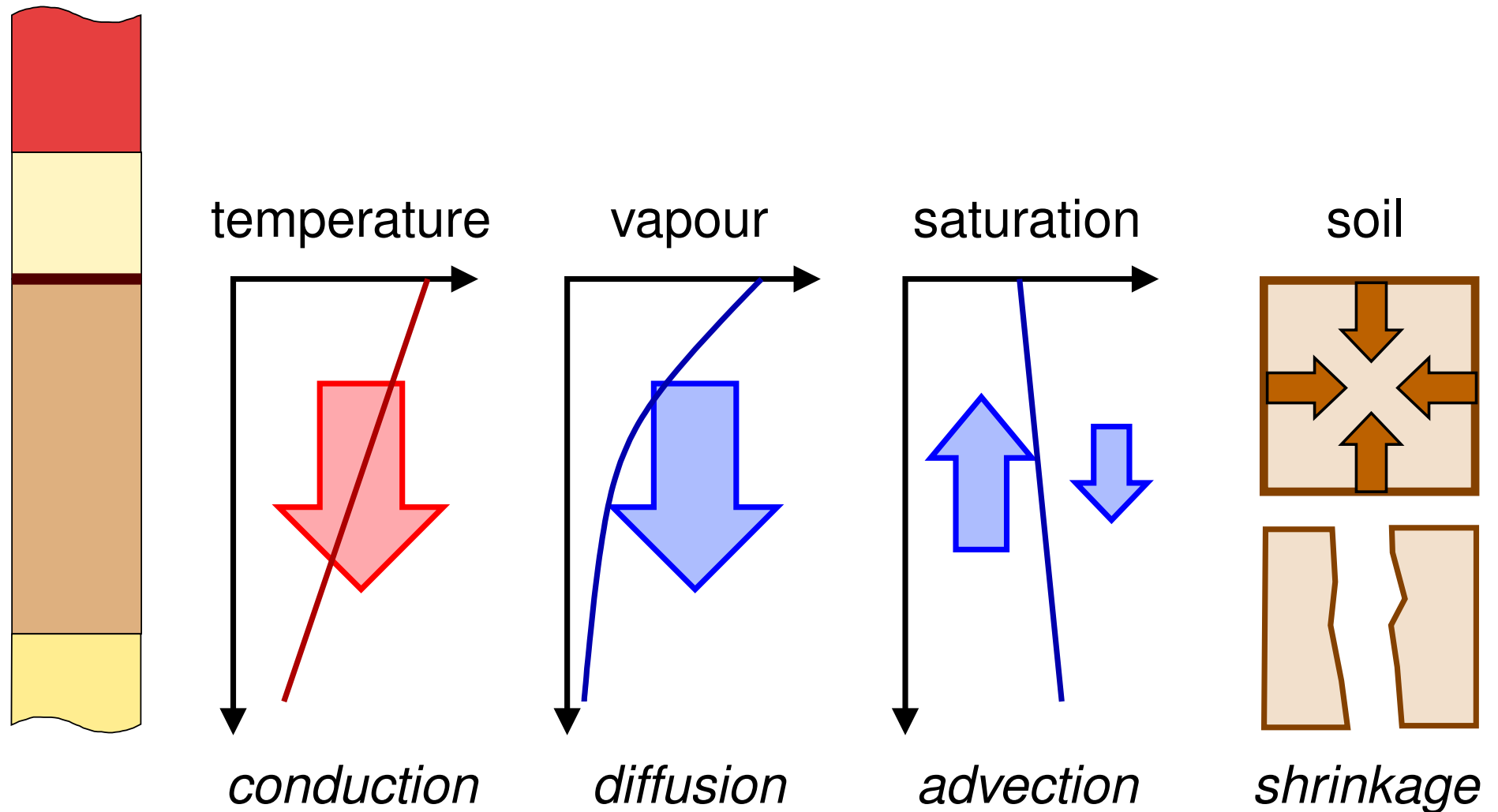
Motivation



Structure of a Base Liner



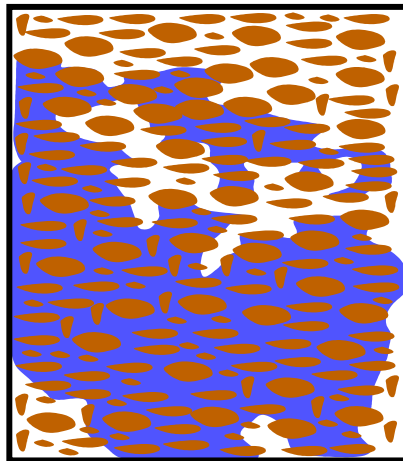
Processes in a Base Liner



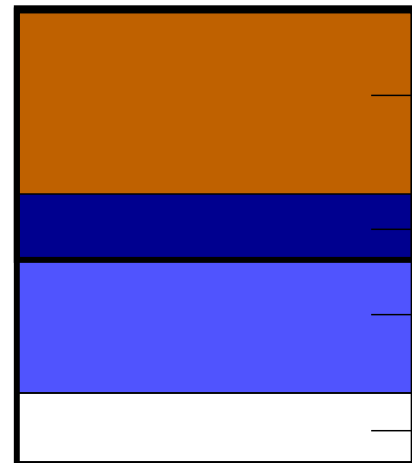
Conceptual Model (1)

constituents

soil, water, air



REV

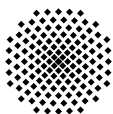


soil matrix

matrix water (immobile)

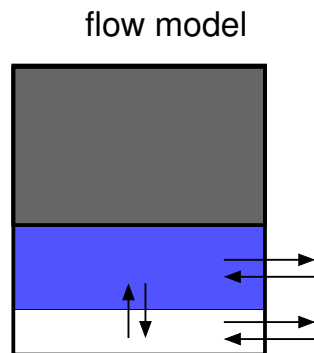
pore water (mobile)

pore gas

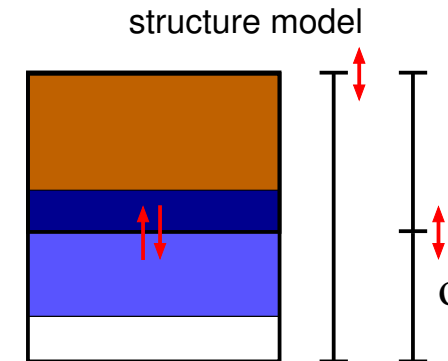


Conceptual Model (2)

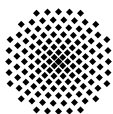
flow and transport



structural alterations

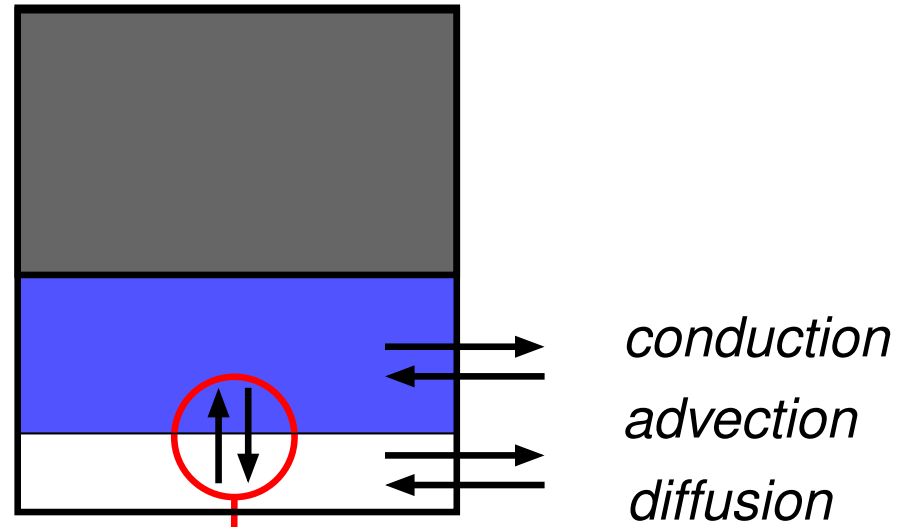


considering flow / transport and structural alterations as two separate, decoupled steps

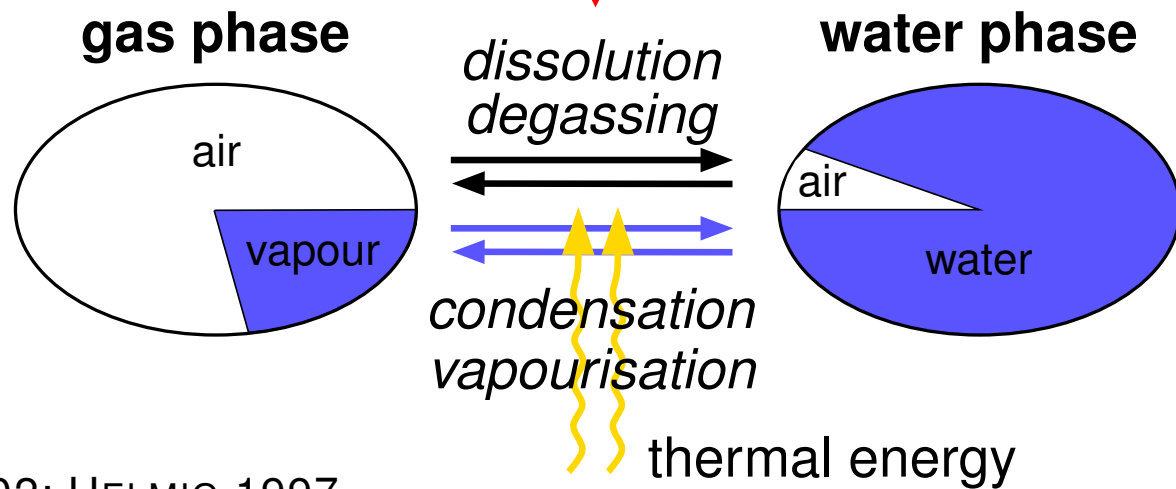


Flow and Transport Model (1)

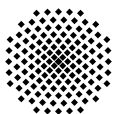
flow and transport



transfer between the phases

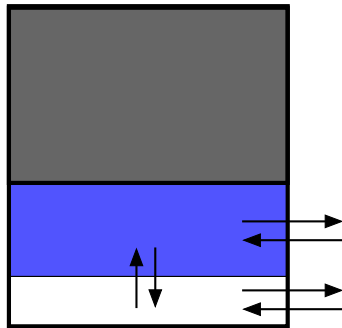


CLASS, HELMIG, BASTIAN 2002; HELMIG 1997

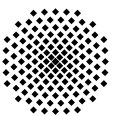


Flow and Transport Model (2)

Assumptions:



- local thermal equilibrium
- chemical equilibrium
- stiff skeleton



Mass Balance Equations

$$K \in \{w, a\}$$

$$\alpha \in \{w, g\}$$

formulation for
each component

→ 2 balance
equations

constraints:

$$S_w + S_g = 1$$

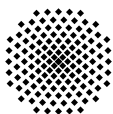
$$p_g = p_w + p_c(S_w)$$

$$\underbrace{\frac{\partial(\sum_{\alpha} \phi \rho_{\alpha}^{mol} x_{\alpha}^K S_{\alpha})}{\partial t}}_{\text{storage}}$$

$$- \underbrace{\sum_{\alpha} \operatorname{div} \left\{ \frac{k_{r\alpha}}{\mu_{\alpha}} \rho_{\alpha}^{mol} x_{\alpha}^K \mathbf{K} (\operatorname{grad} p_{\alpha} - \rho_{mass,\alpha} \mathbf{g}) \right\}}_{\text{advective transport}}$$

$$- \underbrace{\operatorname{div} \left\{ D_{pm}^K \rho_g^{mol} \operatorname{grad} x_g^K \right\}}_{\text{diffusive transport in gas phase}}$$

$$- \underbrace{q^K}_{\text{sink/source}} = 0$$



Balance Equation for Thermal Energy

$$K \in \{w, a\}$$

$$\alpha \in \{w, g\}$$

assumption of
local thermal
equilibrium

→ 1 balance
equation for the
entire fluid-filled,
porous medium

$$\underbrace{\frac{\partial (\sum_{\alpha} \phi \rho_{mass,\alpha} u_{\alpha} S_{\alpha})}{\partial t} + \frac{\partial (1 - \phi) \rho_s c_s T}{\partial t}}_{\text{storage}}$$

storage

$$- \underbrace{\operatorname{div} (\lambda_{pm} \operatorname{grad} T)}_{\text{thermal conduction}}$$

thermal conduction

$$- \underbrace{\sum_{\alpha} \operatorname{div} \left\{ \frac{k_{r\alpha}}{\mu_{\alpha}} \rho_{mass,\alpha} h_{\alpha} \mathbf{K} (\operatorname{grad} p_{\alpha} - \rho_{mass,\alpha} \mathbf{g}) \right\}}_{\text{convective transport}}$$

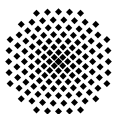
convective transport

$$- \underbrace{\sum_K \operatorname{div} \left\{ D_{pm}^K \rho_{mol,g} h_g^K M^K \operatorname{grad} x_g^K \right\}}_{\text{thermal transport due to diffusion}}$$

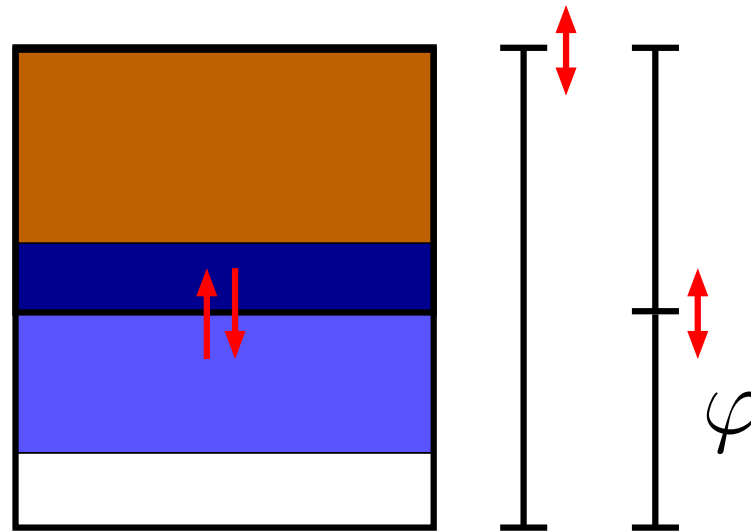
thermal transport due to diffusion

$$- \underbrace{q^h}_{\text{sink/source}} = 0$$

sink/source



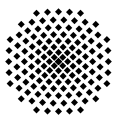
Structural Alterations (1)



*immobilisation /
mobilisation*

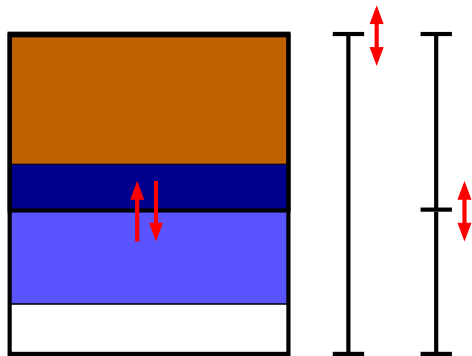
*changes in
volume + porosity*

**adaptation of
hydraulic parameters**

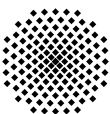


Structural Alterations (2)

key points:



- influence of structural alterations on flow and transport processes ...
- ... by means of adapted hydraulic properties
- ... using constitutive relationships
- rigid soil skeleton
- exclusive of crack formation



Structure Parameter

- swelling / shrinking factor

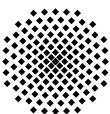
$$\varepsilon = \frac{V}{V_o}$$

- (computationally) effective porosity

$$\varphi_{\text{eff}} = \frac{V_{\text{pore}}}{V_o} = \varphi \varepsilon$$

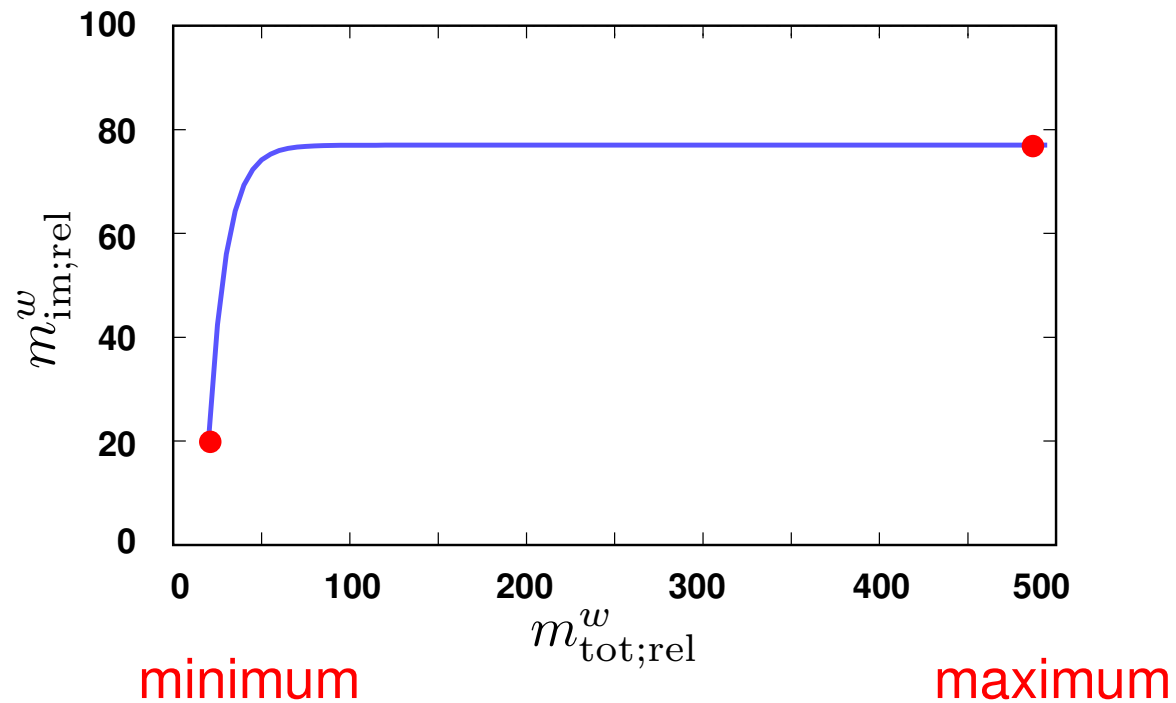
- relative total mass of water

$$m_{\text{tot};\text{rel}}^w = \frac{(n_{\text{im}}^w + n_w^w + n_g^w) M^w}{V}$$

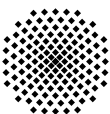


Immobile Matrix Water

$$m_{\text{im};\text{rel}}^w = f_{\text{sat.}}(m_{\text{tot};\text{rel}}^w)$$



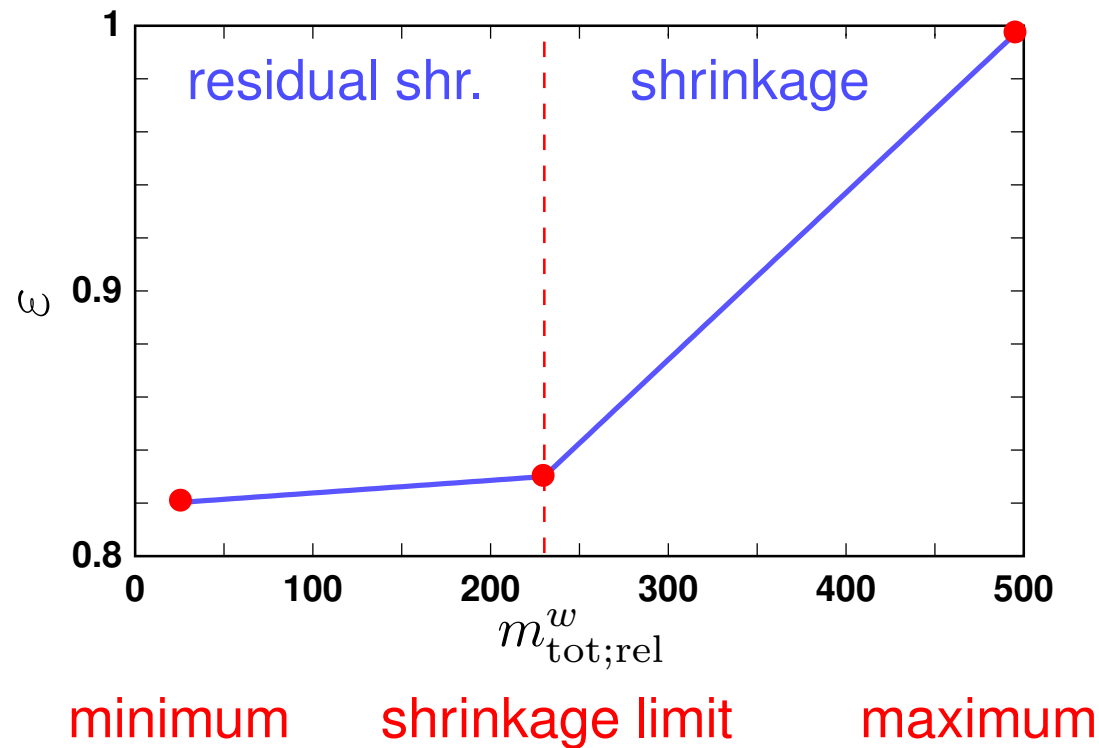
(MEISSNER, DOBROWOLSKY 2003)



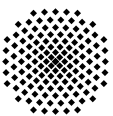
Shrinking Factor

$$\varepsilon = f_{\text{linear; residu}}(m_{\text{tot;rel}}^w)$$

$$\varepsilon = f_{\text{linear; schrumpf}}(m_{\text{tot;rel}}^w)$$



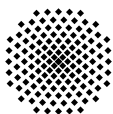
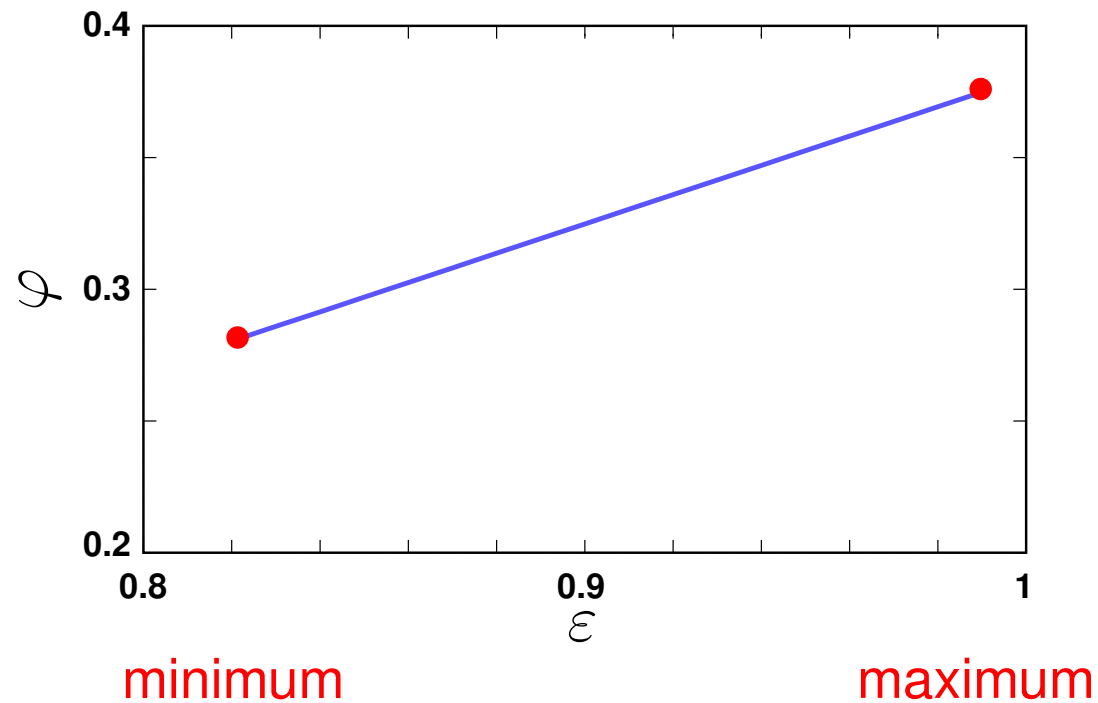
(e.g. BRAUNS, SCHNEIDER, GOTTHEIL 2000)



Porosity

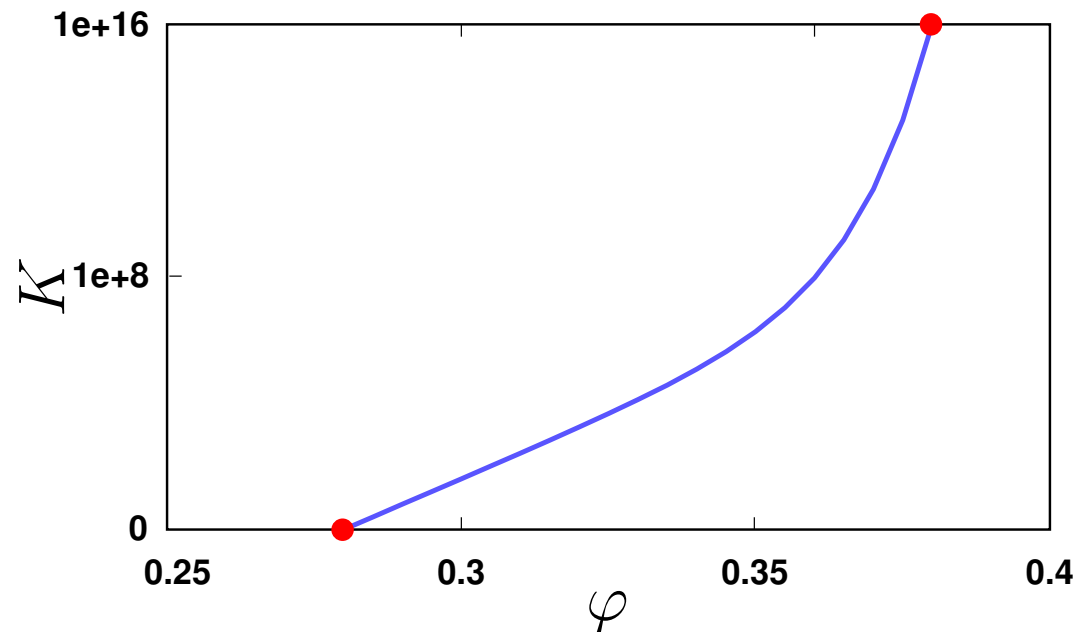
a) $\varphi = f(m_{\text{tot};\text{rel}}^w)$

b) $\varphi = f_{\text{linear}}(\varepsilon)$

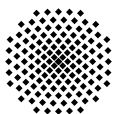


Permeability

$$K = f(\varphi)$$

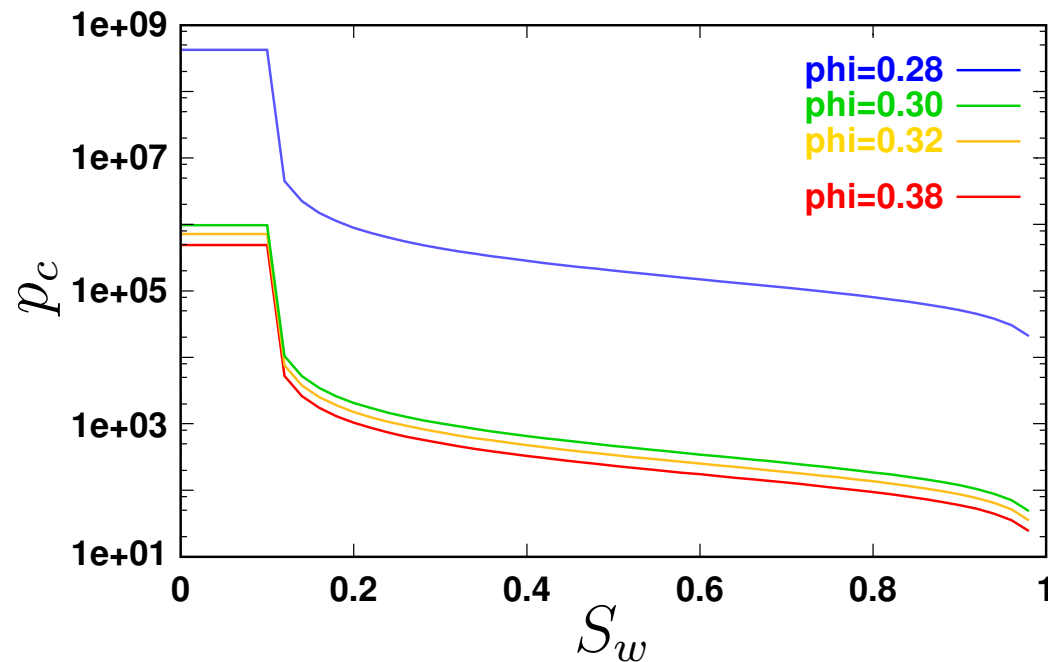


(e.g. CLAUSER 2003)

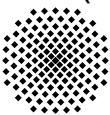


Capillary Pressure

$$p_c(S_w) = p_{c;\text{ref}}(S_w) \sqrt{\frac{K_{\text{ref}}}{K} \frac{\varphi}{\varphi_{\text{ref}}}}$$

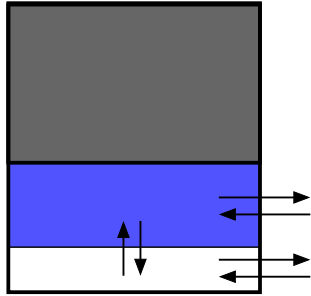


(LEVERETT 1941)



Coupling Flow + Structural Alterations

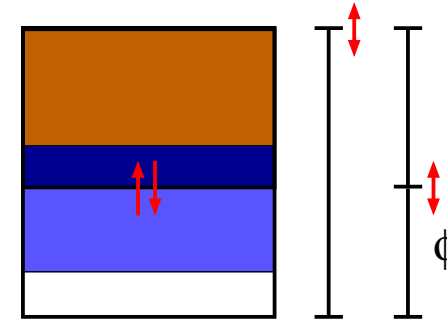
flow and transport



1st step within one time step

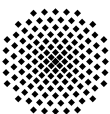
- compute flow and transport
- compute mass of water, mass of air and energy

structural alterations

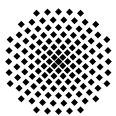
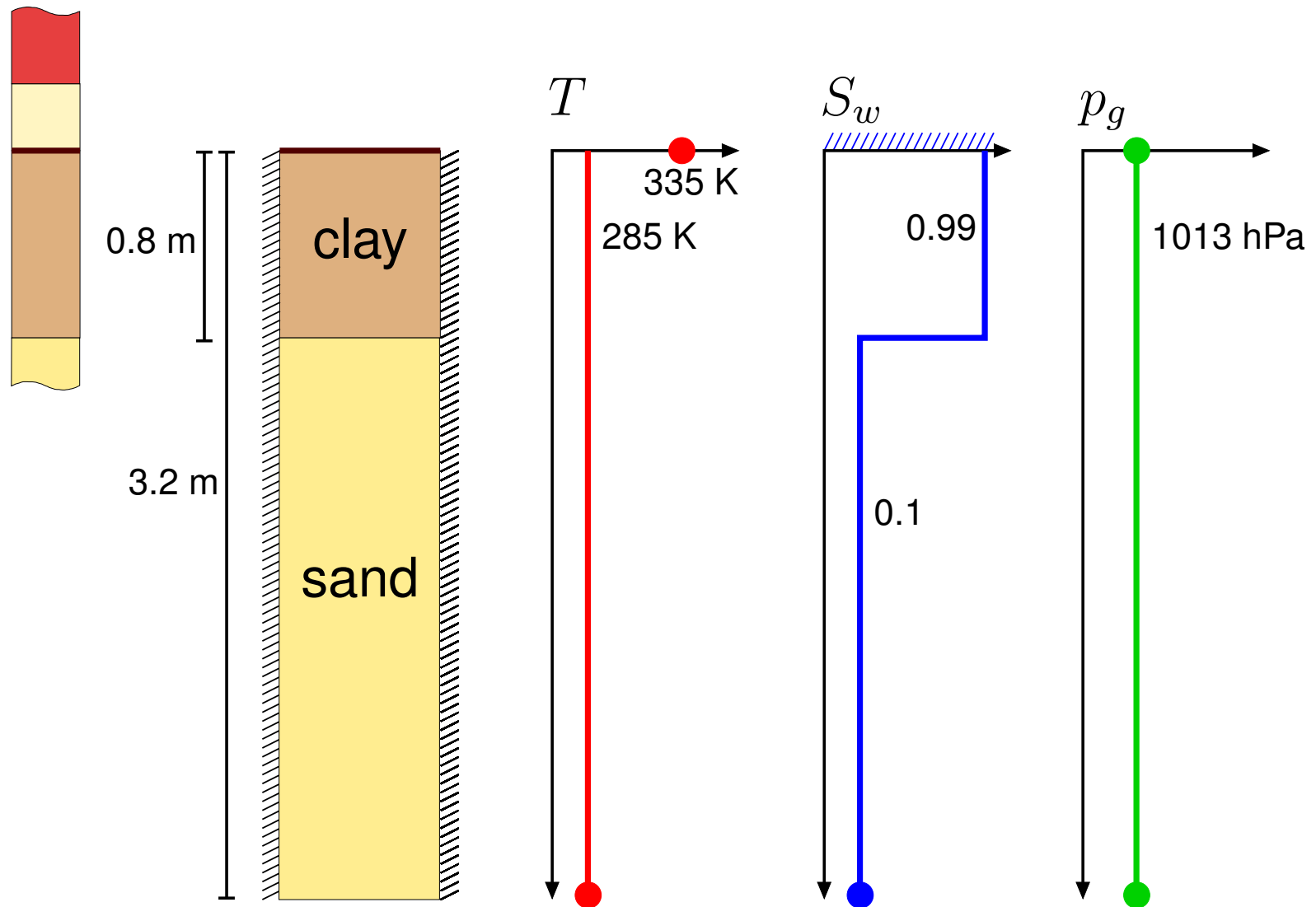


2nd step within one time step

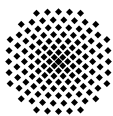
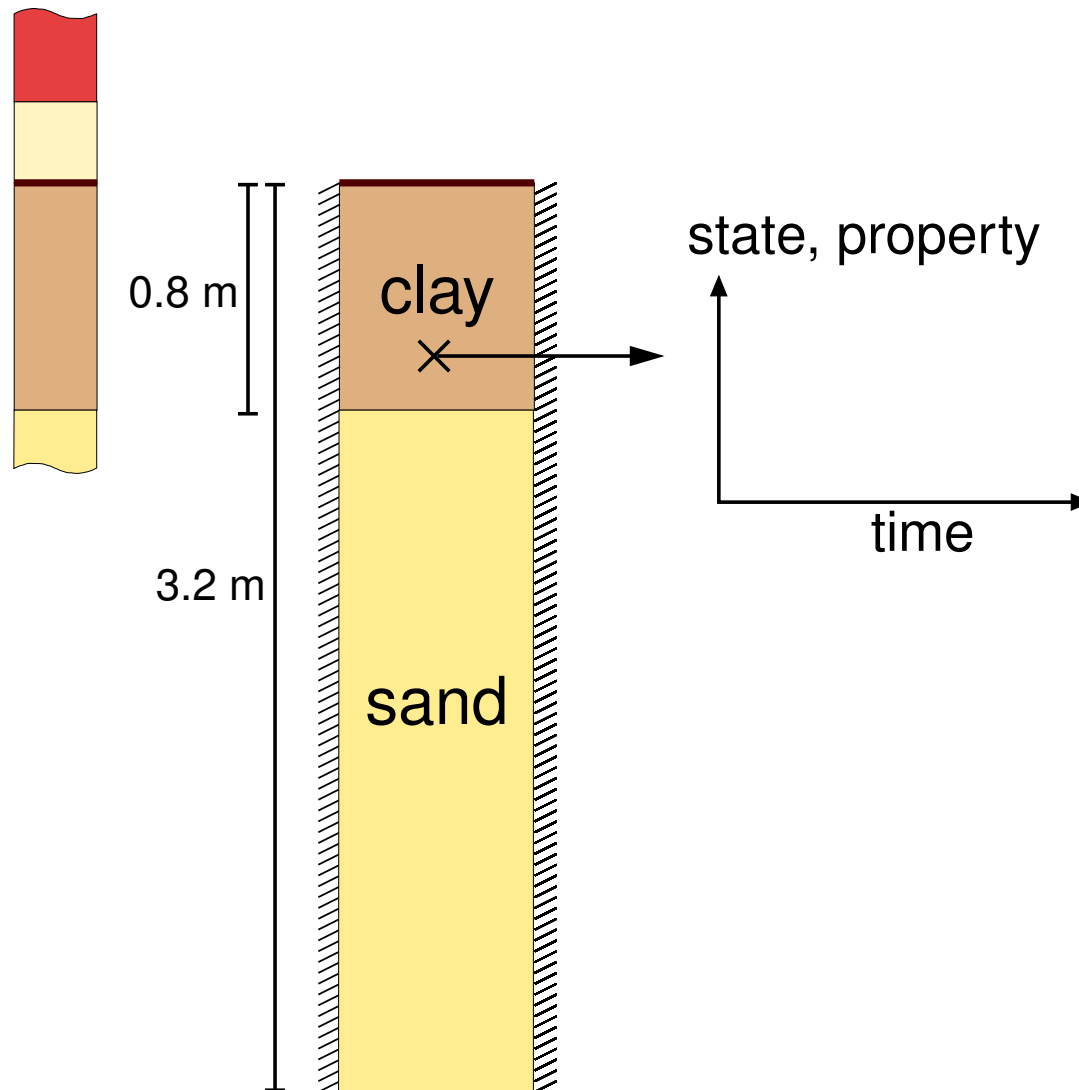
- update structure parameters
- compute new state variables while maintaining mass and energy conservation and thermodynamic equilibrium



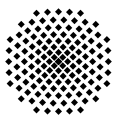
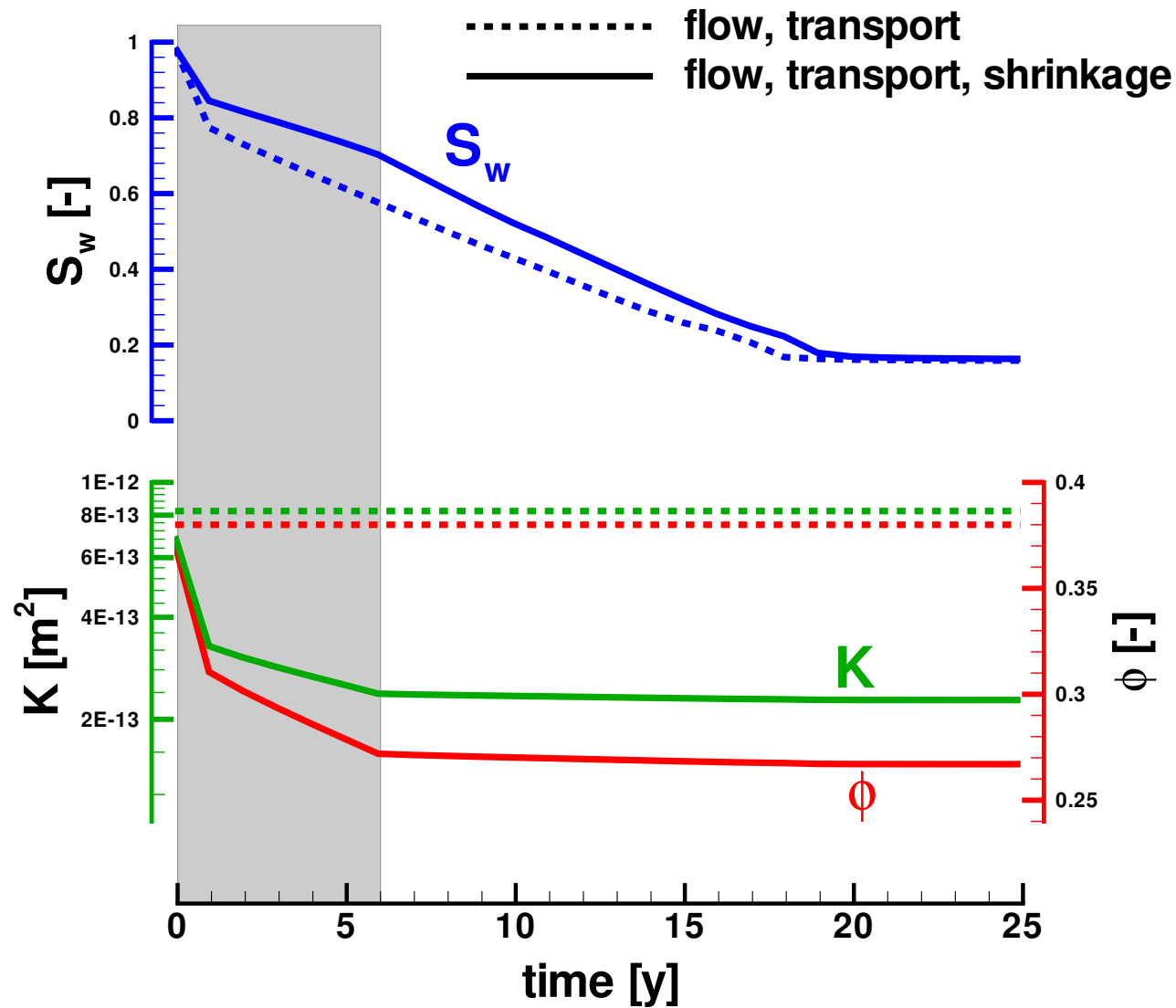
Model Comparison (1)



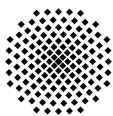
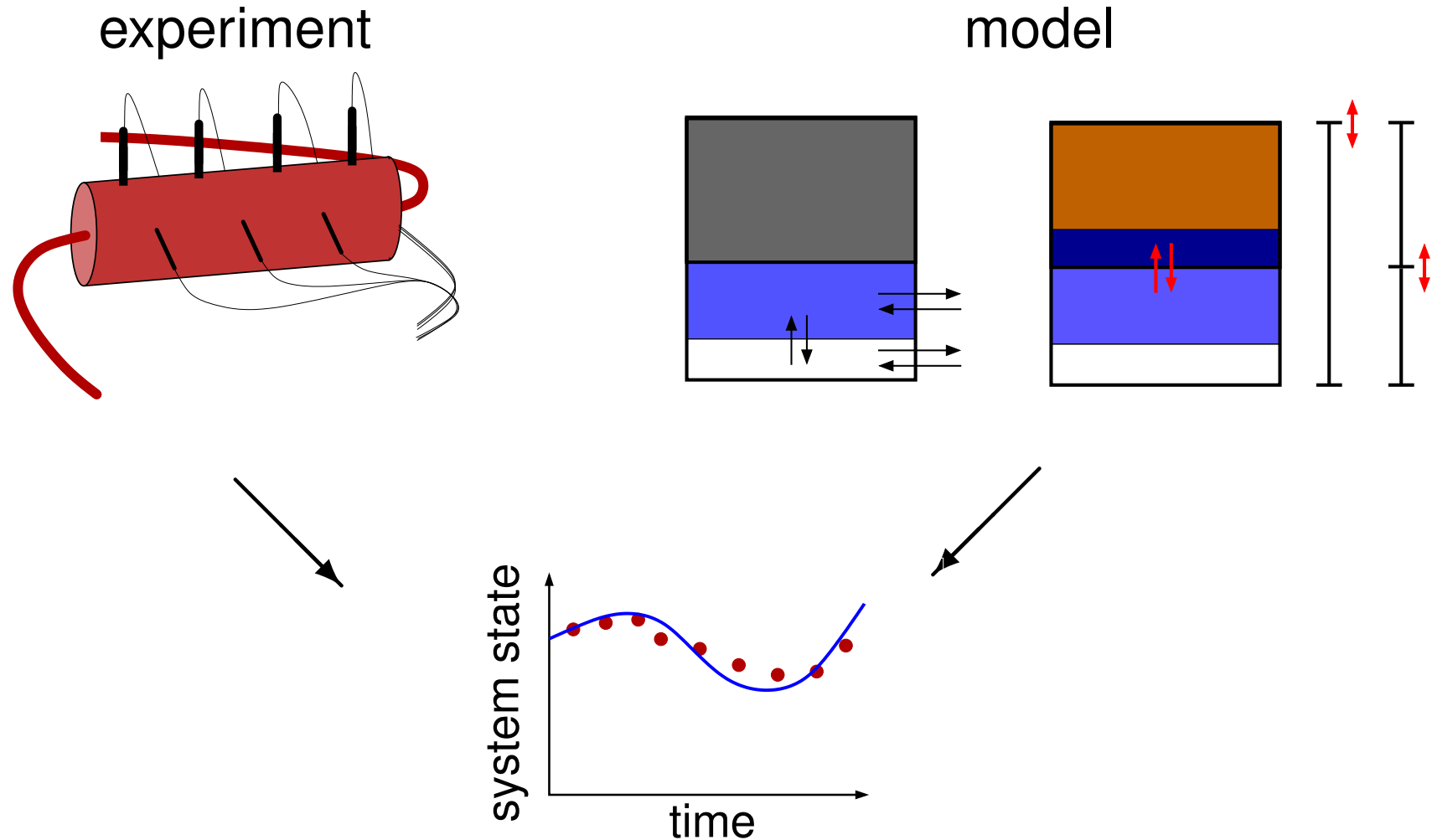
Model Comparison (1)



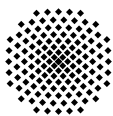
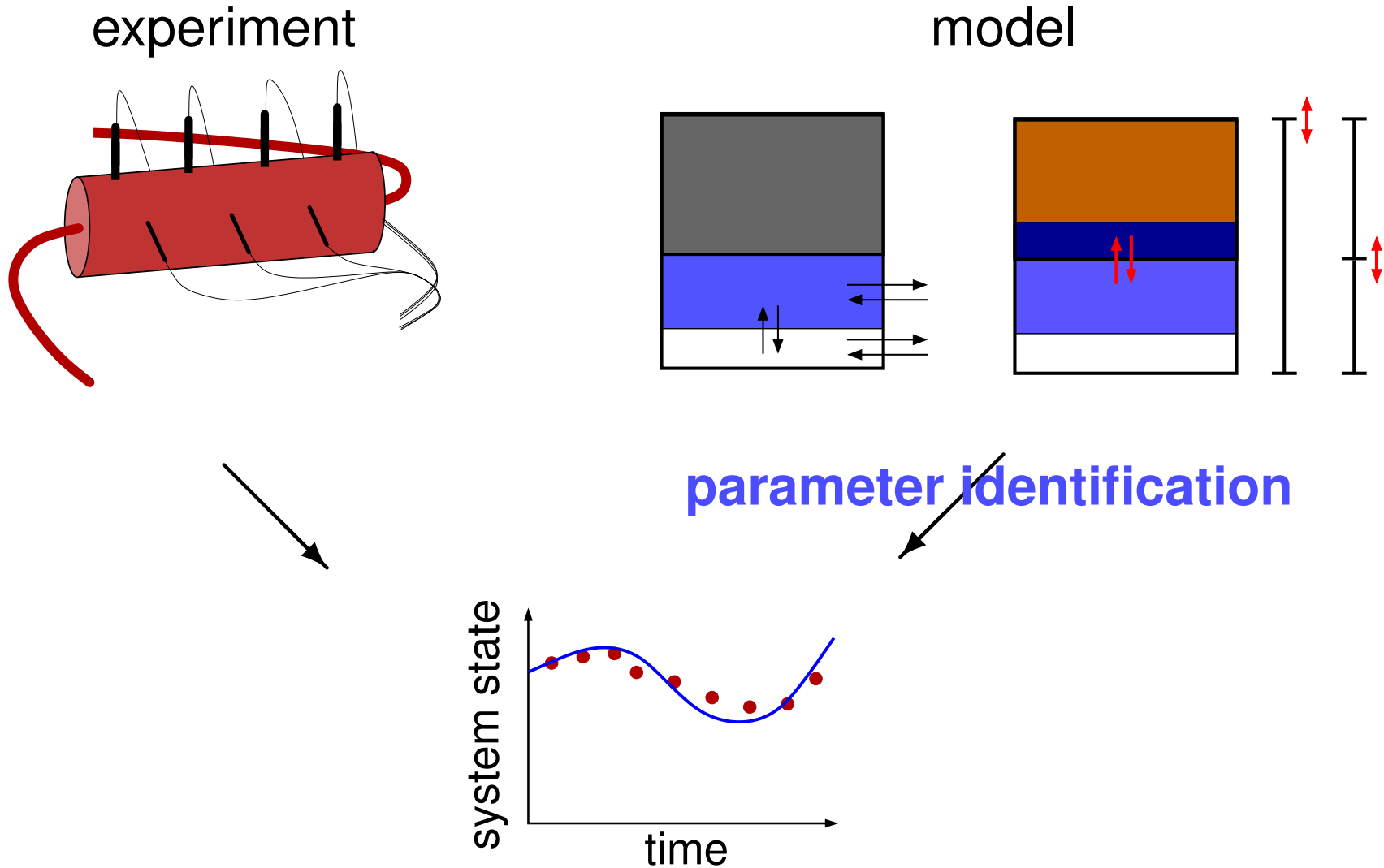
Model Comparison (2)



Model Calibration and Validation



Model Calibration and Validation



Final Remarks

- model concept that includes – on a phenomenological basis (rigid porous matrix) – the effects of swelling/shrinking within a non-isothermal multiphase multicomponent flow and transport model
- integration of additional constitutive relationships into existing model
- application example shows reasonable results
- comparison with experimental data in preparation
- parameter-identification strategy requires further development

