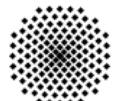

Reliability of numerical models for simulating CO₂ storage in deep geological formations

Holger Class,
Anozie Ebigbo, Andreas Kopp, Rainer Helmig

DGG 2007, Aachen, March 28th, 2007



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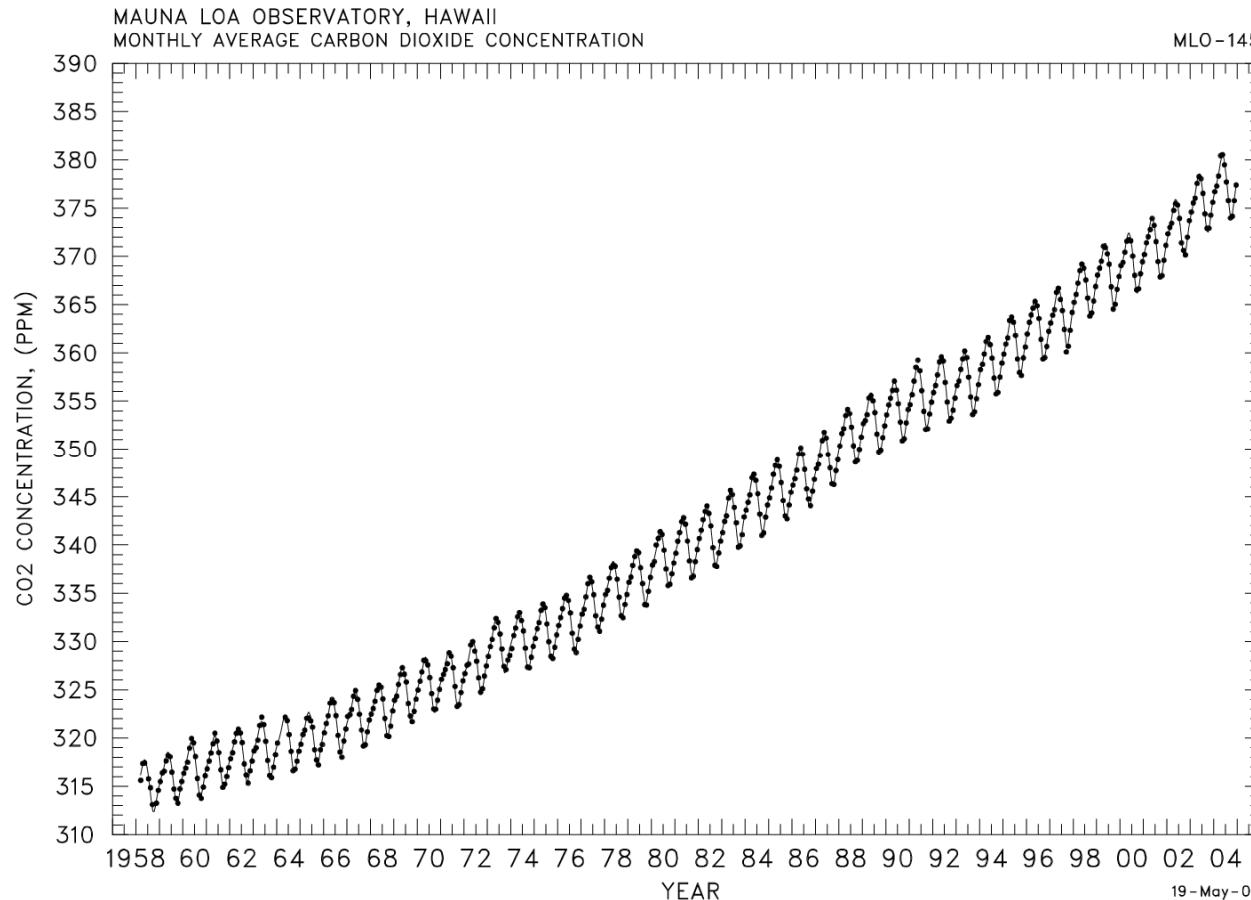
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"Numerical Simulation of CO₂ Sequestration in Geological Formations", CMWR Copenhagen, June 20, 2006

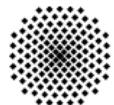


Atmospheric CO₂ Concentration

Increase in atmospheric CO₂ concentration is causing global climate change since CO₂ is a greenhouse gas.



Keeling & Whorf, 2005



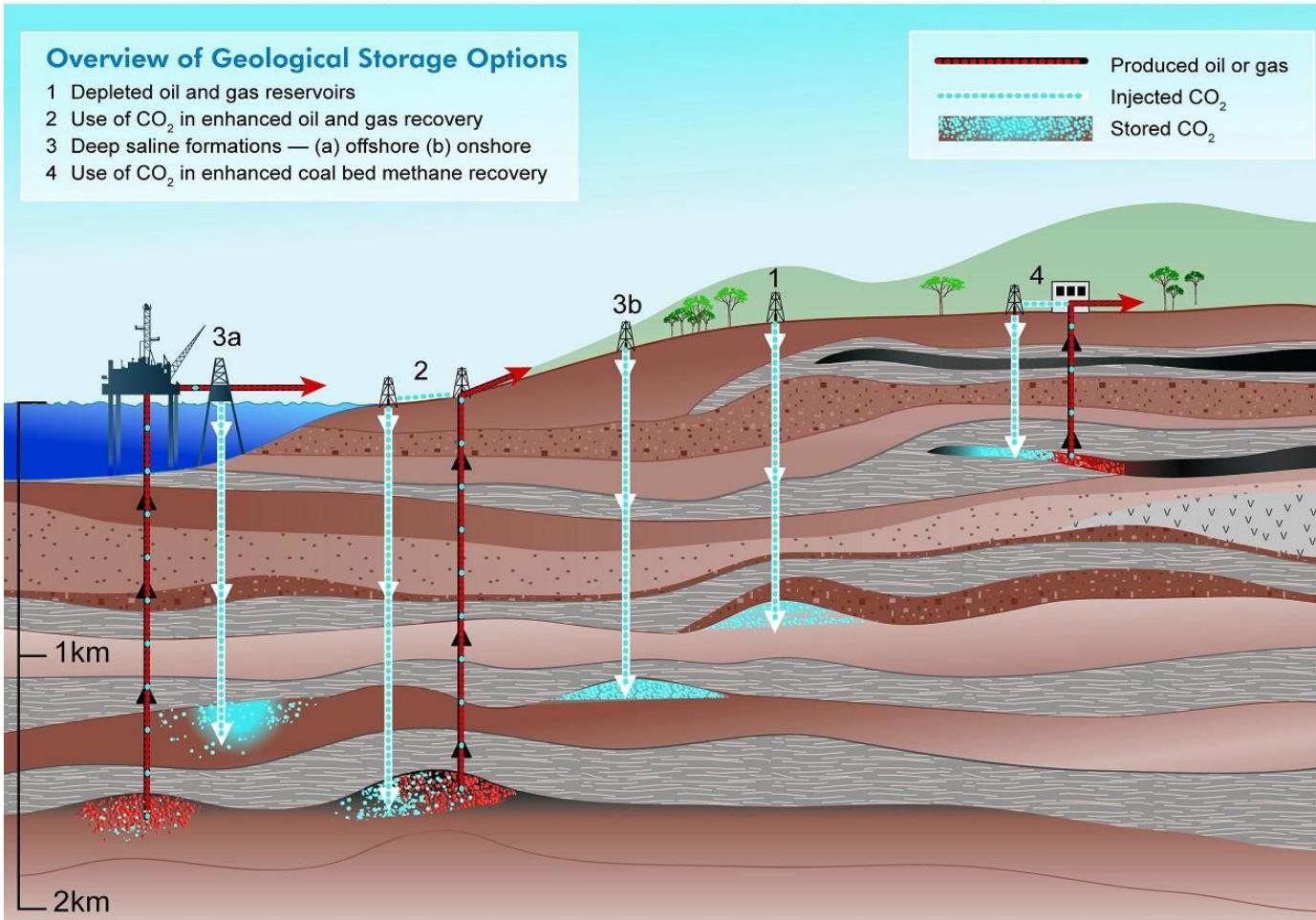
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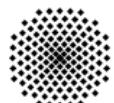
"Numerical Simulation of CO₂ Sequestration in Geological Formations", CMWR Copenhagen, June 20, 2006



Geological Storage Options



© Intergovernmental Panel on Climate Change (2006)



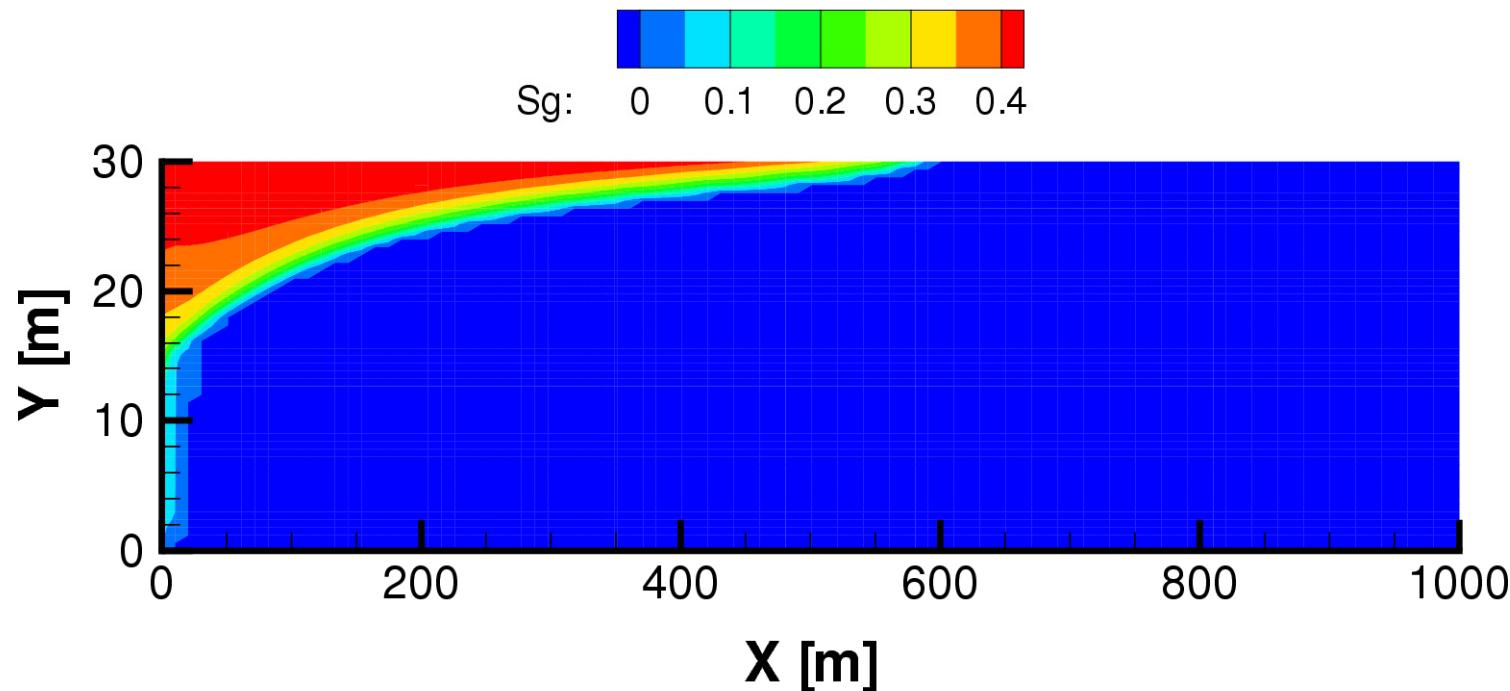
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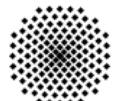
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CO₂-injection



- Interface depends on injection rate, aquifer structure and fluid properties (viscosities, densities).



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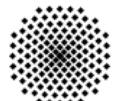
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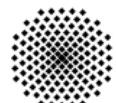
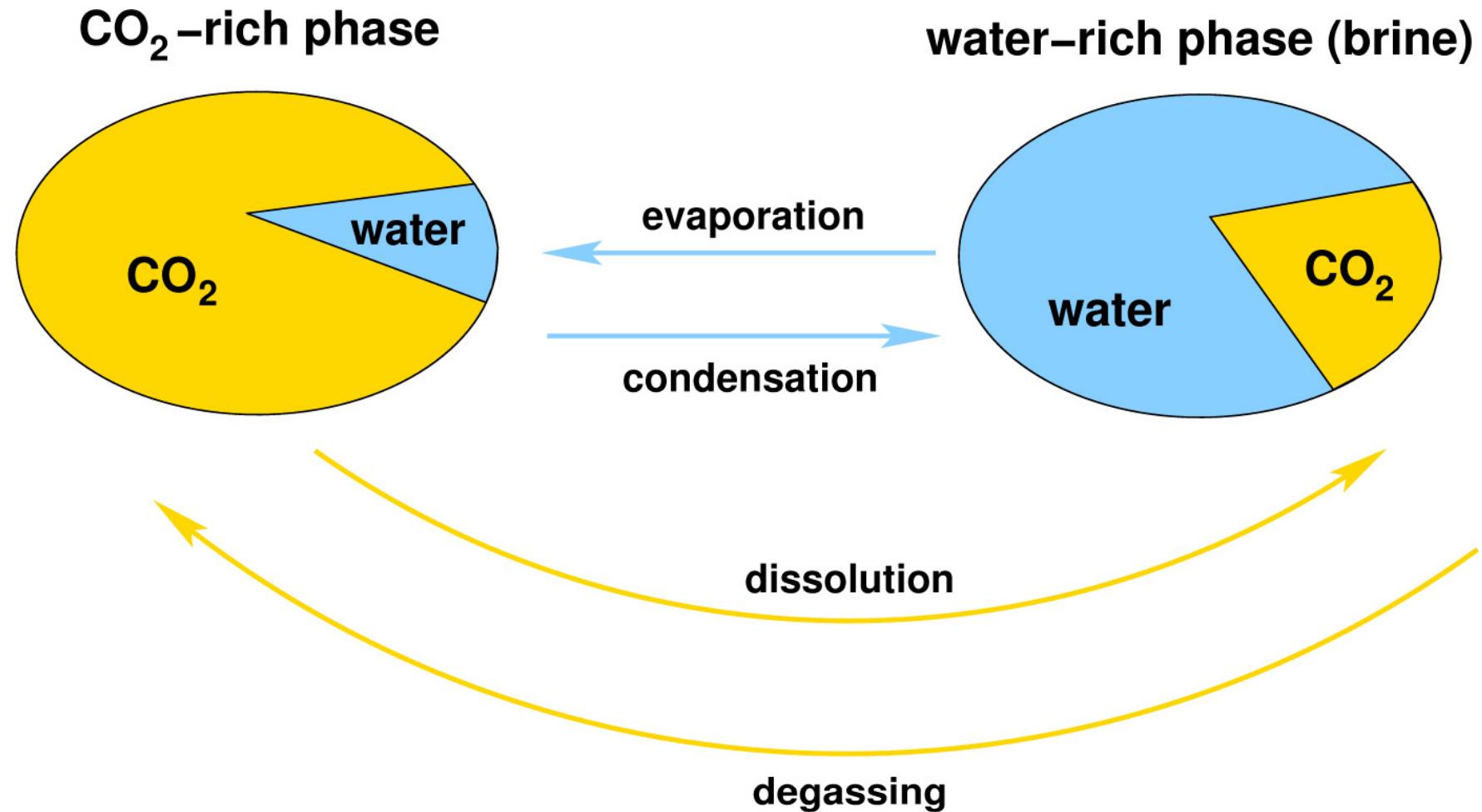
Model: Main Assumptions

General assumptions

- Slow velocities (Reynolds number < 1)
- Local thermodynamical equilibrium
 - thermal
 - mechanical
 - chemical
- Rock matrix is rigid
 - porosity $\phi = f(\mathbf{x})$, $\phi \neq f(t)$
 - permeability $\mathbf{K} = f(\mathbf{x})$, $\mathbf{K} \neq f(t)$

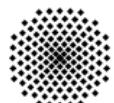


Model Concept: Two-Phase Two-Component

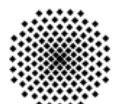
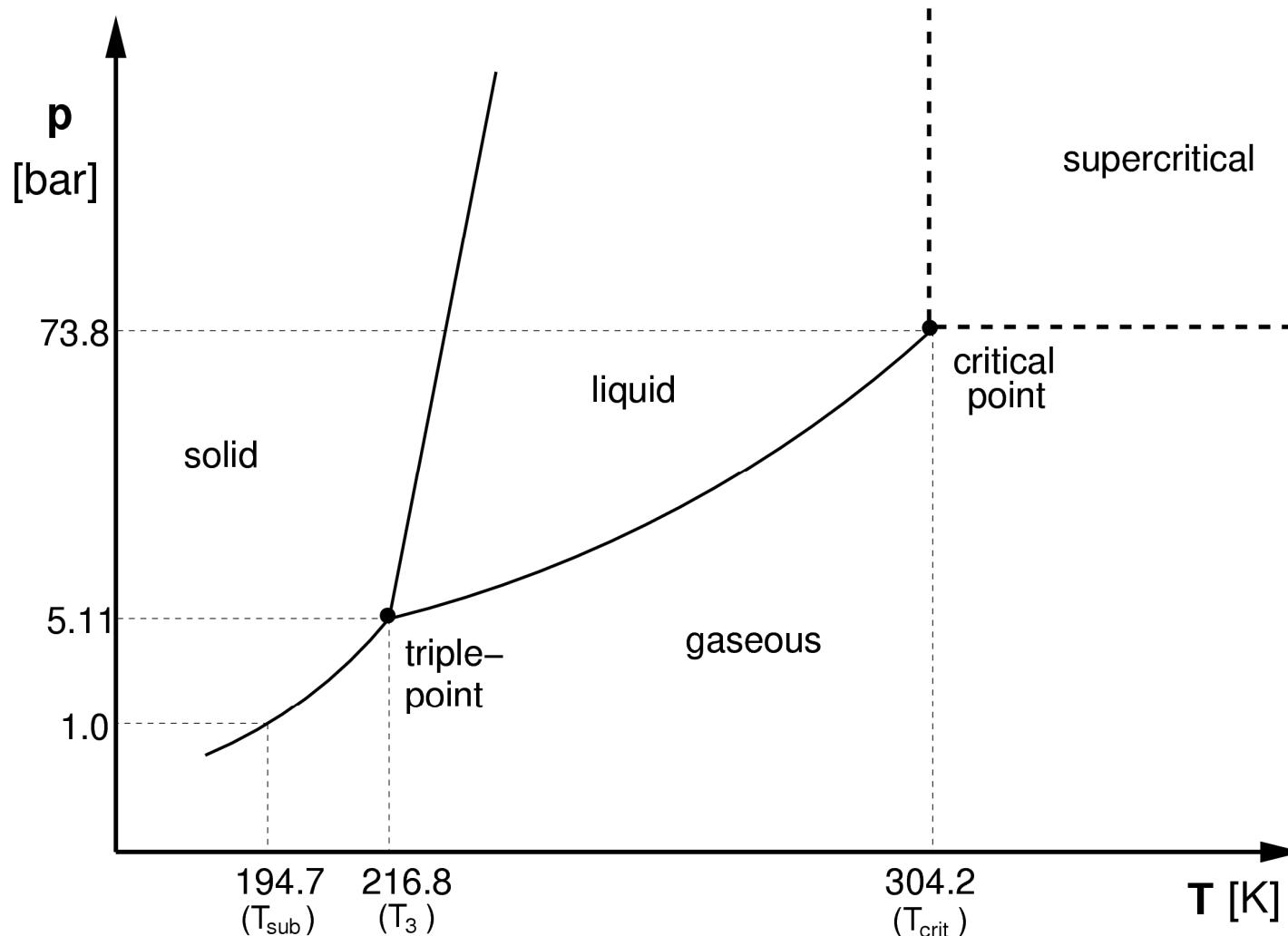


Model Assumptions

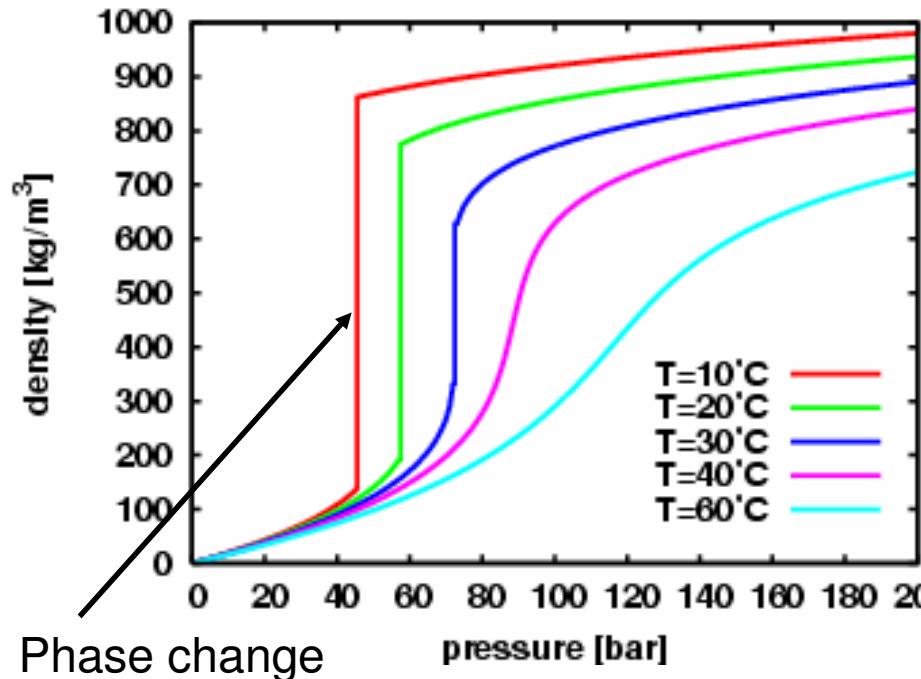
- Two fluid phases in a rigid rock matrix: CO₂ and brine
- Salinity influences brine fluid properties but does not change with time $S = f(\mathbf{x})$, $S \neq f(t)$
- Diffusion only in the brine phase
- Multi-phase behavior is taken into account by
 - Capillary pressure-saturation relationships $p_c = f(S_\alpha, \mathbf{x})$
 - Relative permeability-saturation relationship $k_{r\alpha} = f(S_\alpha, \mathbf{x})$
- No chemical reactions with rock matrix and no geomechanical effects



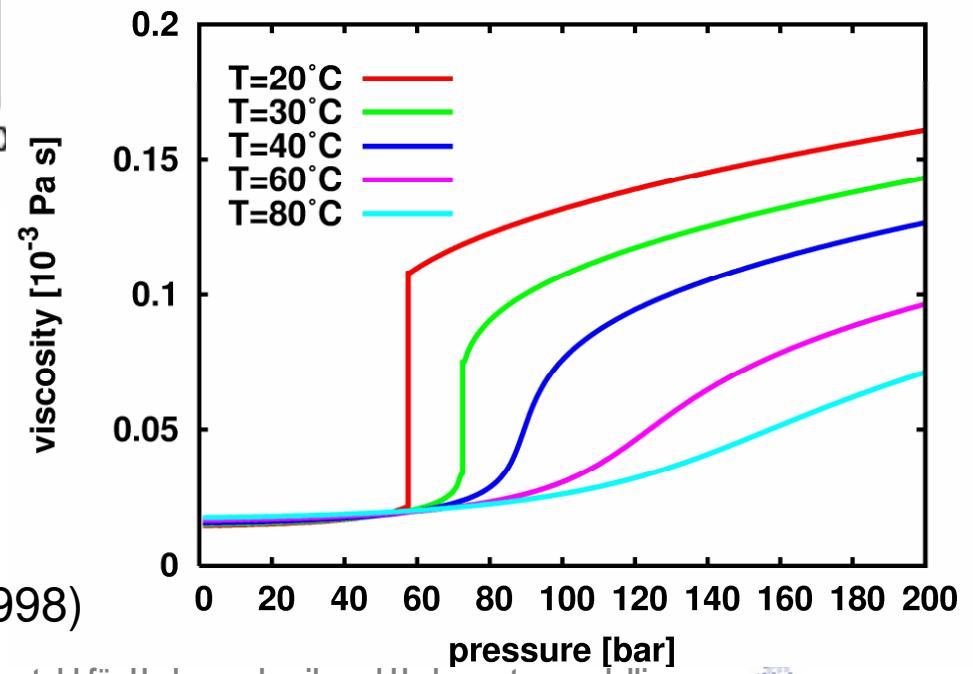
CO₂ Phase Diagram



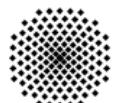
Density and viscosity of CO₂



(Span & Wagner, 1996)



(Fenghour et al, 1998)



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Model: Mass Balance Equations

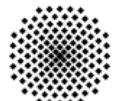
$$\underbrace{\phi \frac{\partial (\sum_{\alpha} \rho_{\alpha} X_{\alpha}^C S_{\alpha})}{\partial t}}_{\text{storage}}$$

Two mass balance equations
for components CO₂ and water

$$-\underbrace{\sum_{\alpha} \nabla \cdot \left\{ \frac{k_{r\alpha}}{\mu_{\alpha}} \rho_{\alpha} X_{\alpha}^C \mathbf{K} (\nabla p_{\alpha} - \rho_{\alpha} \mathbf{g}) \right\}}_{\text{advective transport}}$$

$$-\underbrace{\nabla \cdot \left\{ D_{pm}^C \rho_b \nabla X_b^C \right\}}_{\text{diffusive transport}}$$

$$- \underbrace{q^C}_{\text{source/sink}} = 0 \quad C \in \{w, CO_2\}, \alpha \in \{b, CO_2\}$$



Model: Energy Balance Equation

$$\underbrace{\phi \frac{\partial (\sum_{\alpha} \rho_{\alpha} u_{\alpha} S_{\alpha})}{\partial t} + (1 - \phi) \frac{\partial \rho_s c_s T}{\partial t}}_{\text{storage}}$$

One energy balance equation,
assumption: local thermal
equilibrium

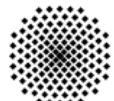
$$-\underbrace{\nabla \cdot (\lambda_{pm} \nabla T)}_{\text{heat conduction}}$$

$$-\sum_{\alpha} \nabla \cdot \left\{ \frac{k_{r\alpha}}{\mu_{\alpha}} \rho_{\alpha} h_{\alpha} \mathbf{K} (\nabla p_{\alpha} - \rho_{\alpha} \mathbf{g}) \right\}$$

heat transport due to advection

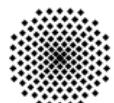
$$-\sum_{\text{C}} \nabla \cdot \left\{ D_{pm}^{\text{C}} \rho_b h_b^{\text{C}} \nabla X_b^{\text{C}} \right\} - \underbrace{q^h}_{\text{source/sink}} = 0$$

heat transport due to diffusion



Numerical Model

- Time discretization: fully implicit Euler scheme
- Space discretization: BOX-method, node-centered finite volume method (locally mass conservative, unstructured grid)
- Linearization: Newton-Raphson method
- Several linear solvers available (e.g. Multigrid)
- Model runs parallel



Model testing – validation/verification

The model is running – what's next??

Apply it to the field-scale,
solve the problems and
produce colorful pictures

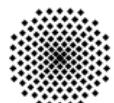
← *the self-confident way*

or

the self-critical way



Develop a strategy to
improve the confidence in
the model and then go to
the field-scale



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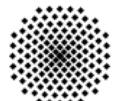


Model testing – validation/verification

Why should there be doubts concerning reliability?

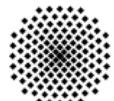
- Capillary pressure and relative permeabilities
- Fluid properties (density, viscosity, enthalpy)
- Phase behavior (dissolution, evaporation)
- Influence of other components (e.g. salt, non-pure CO₂, etc.)
- Justification of the model assumptions

- Mathematical and numerical solution methods (discretization, meshing, etc.)
- ...?

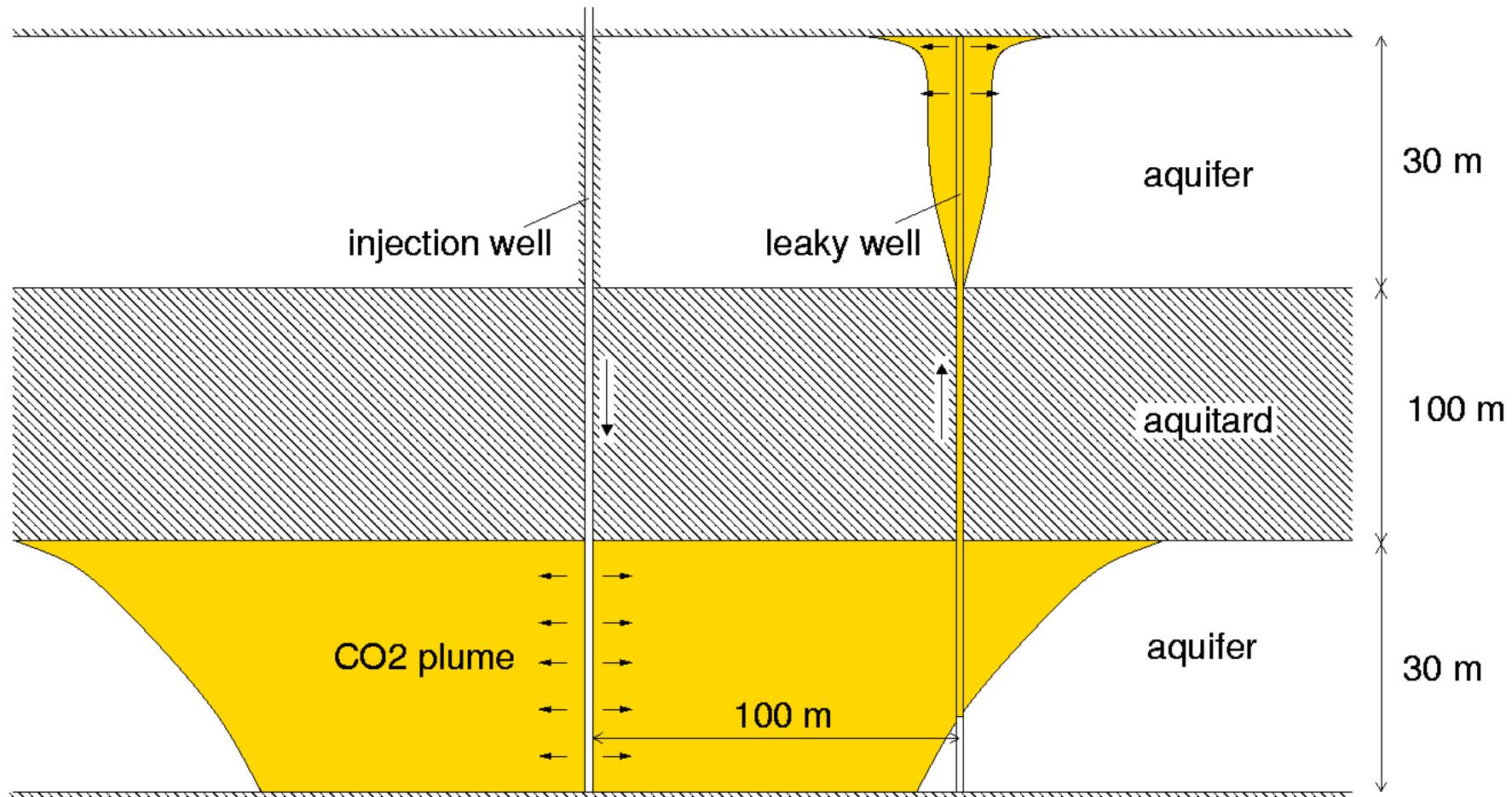


Benchmark Example

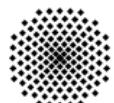
- CO₂ injection into an aquifer,
- subsequent plume evolution and
- leakage through an abandoned/leaky well.



Benchmark Example



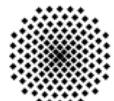
Leakage scenario from *Nordbotten et al. 2005*



Simulation(1)

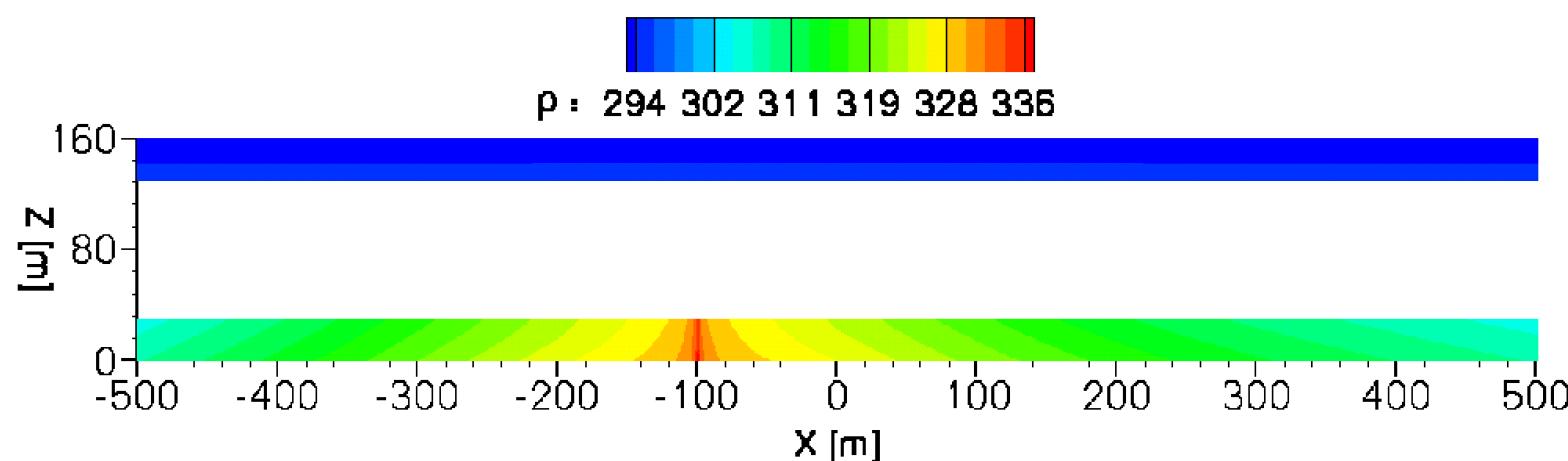
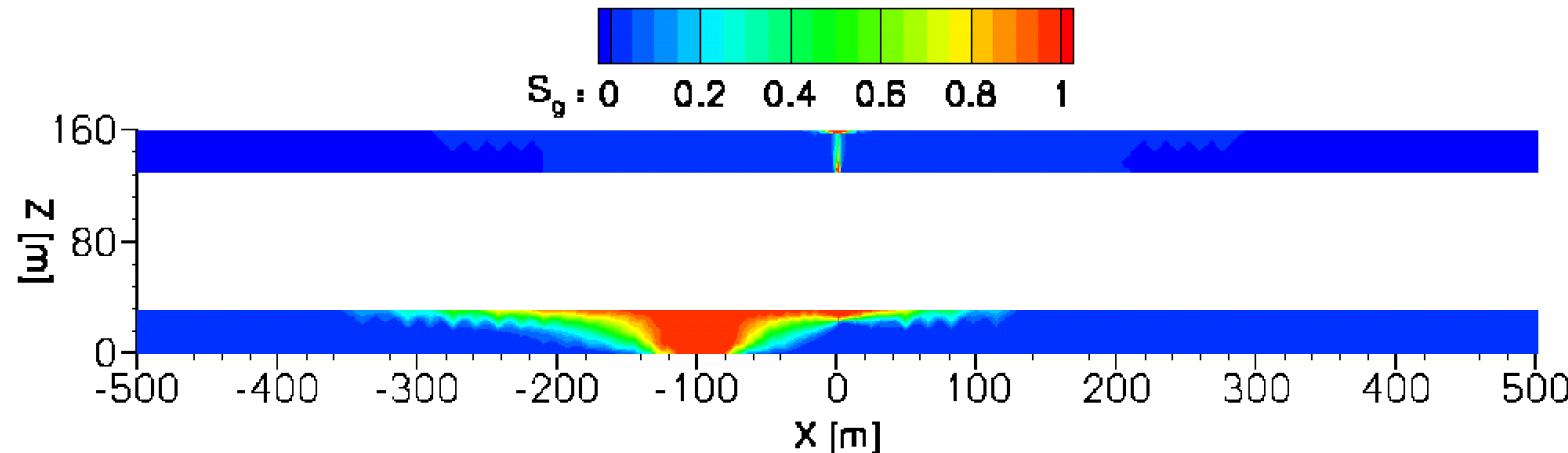
Comparison of numerical simulation
with semi-analytical solution (by *Nordbotten et al. 2005*)

- Domain dimensions: 1000 m x 1000 m x 160 m
 - Aquifer permeability: 20 mD
 - CO₂ injection rate: 8.87 kg/s
 - Distance between wells: 100 m
-
- **Aquifer depth: Between 2840 m and 3000 m**
 - **Constant fluid properties; isothermal; no dissolution**

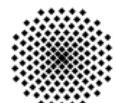


Simulation(1) : Results

Saturation



Pressure [bar]



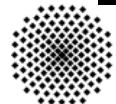
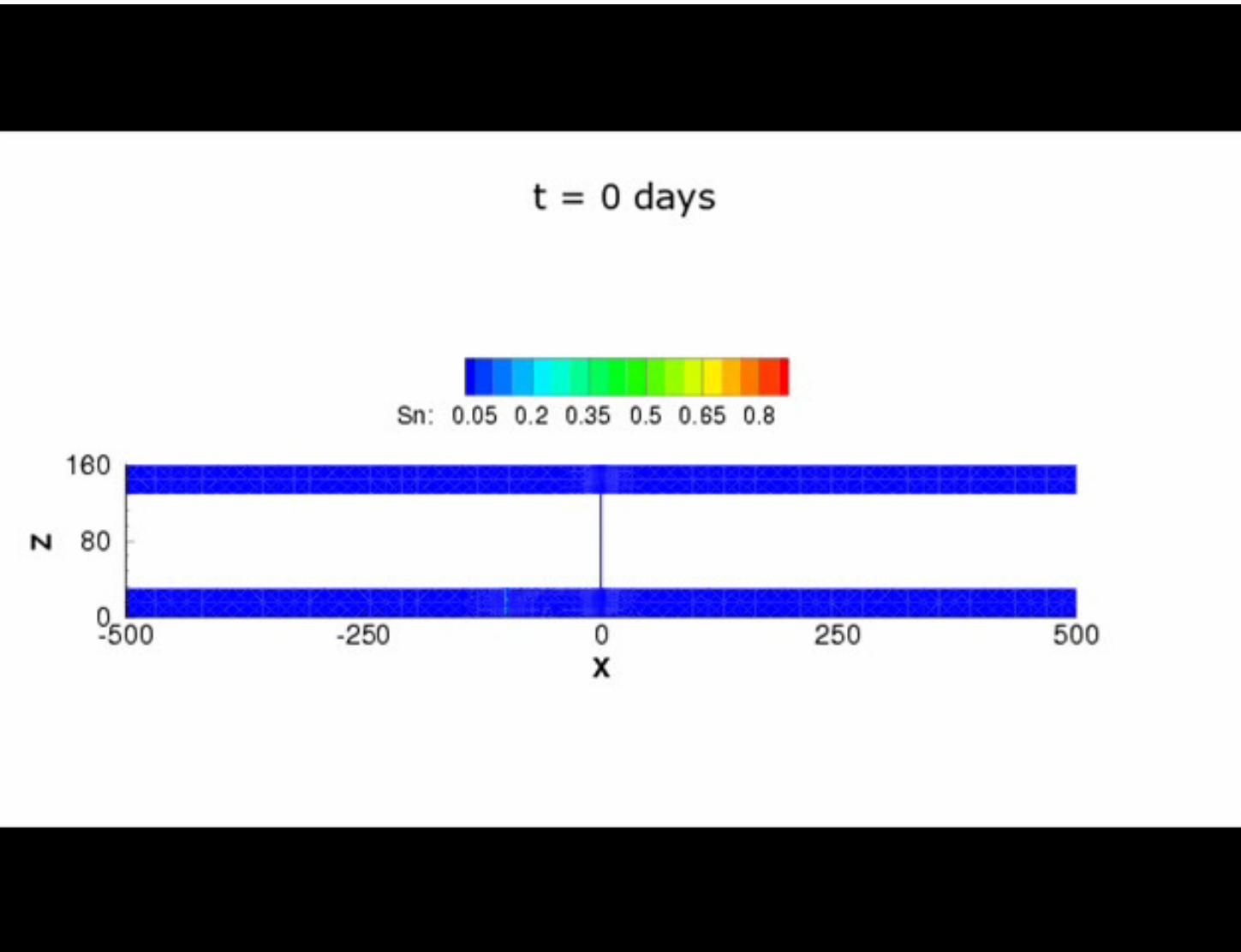
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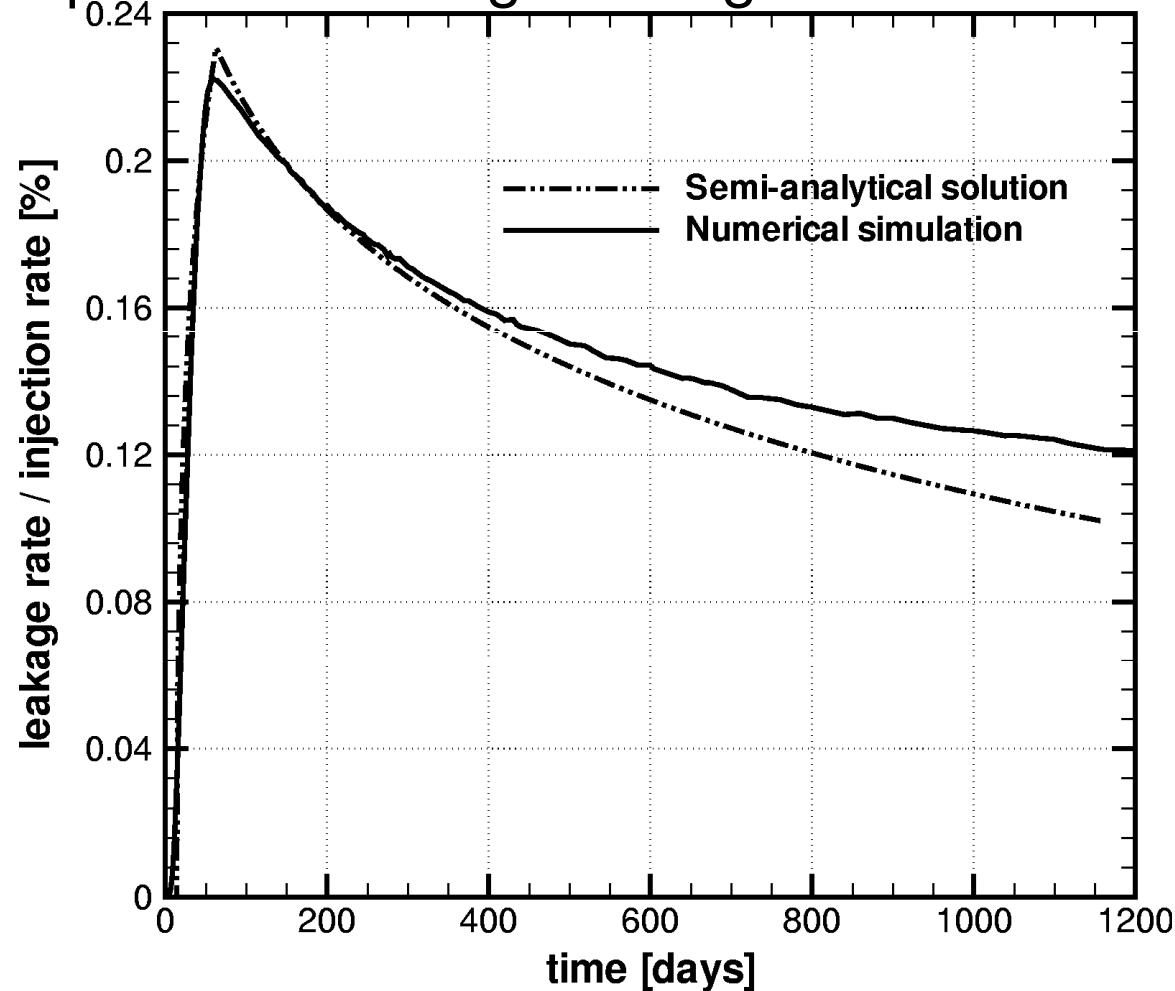


Simulation (1): Results

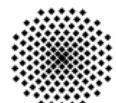


Simulation(1): Results

Comparison: Leakage through abandoned well



Ebigbo et al., 2006 (Computational Geosciences)



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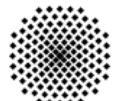
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Simulation(2)

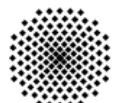
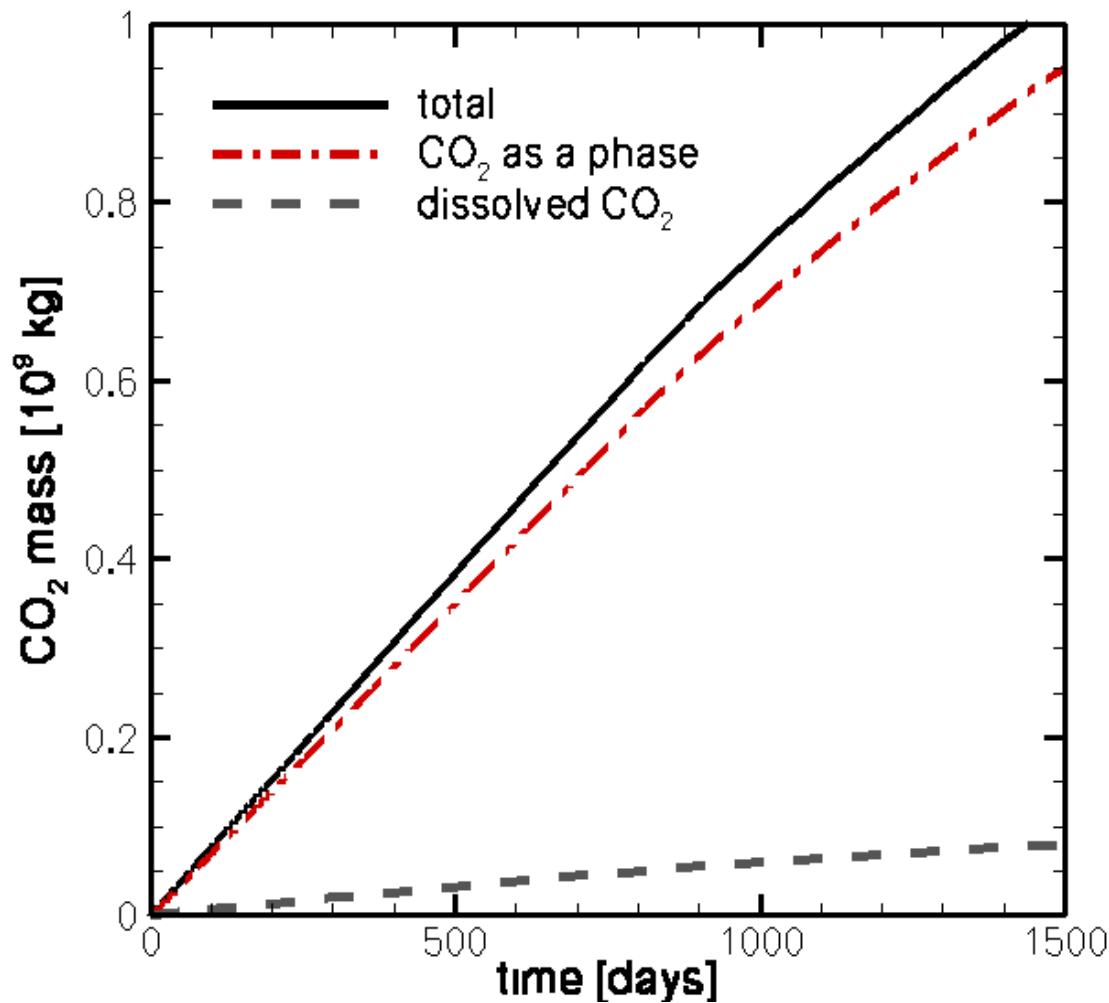
Including dissolution and thermal effects

- Domain dimensions: 1000 m x 1000 m x 160 m
 - CO₂ injection rate: 8.87 kg/s
 - Distance between wells: 100 m
 - **Aquifer depth: Between 640 m and 800 m**
 - **Fluid properties depend on T , p and phase composition; non-isothermal; CO₂ can dissolve in brine**
-



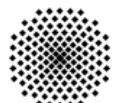
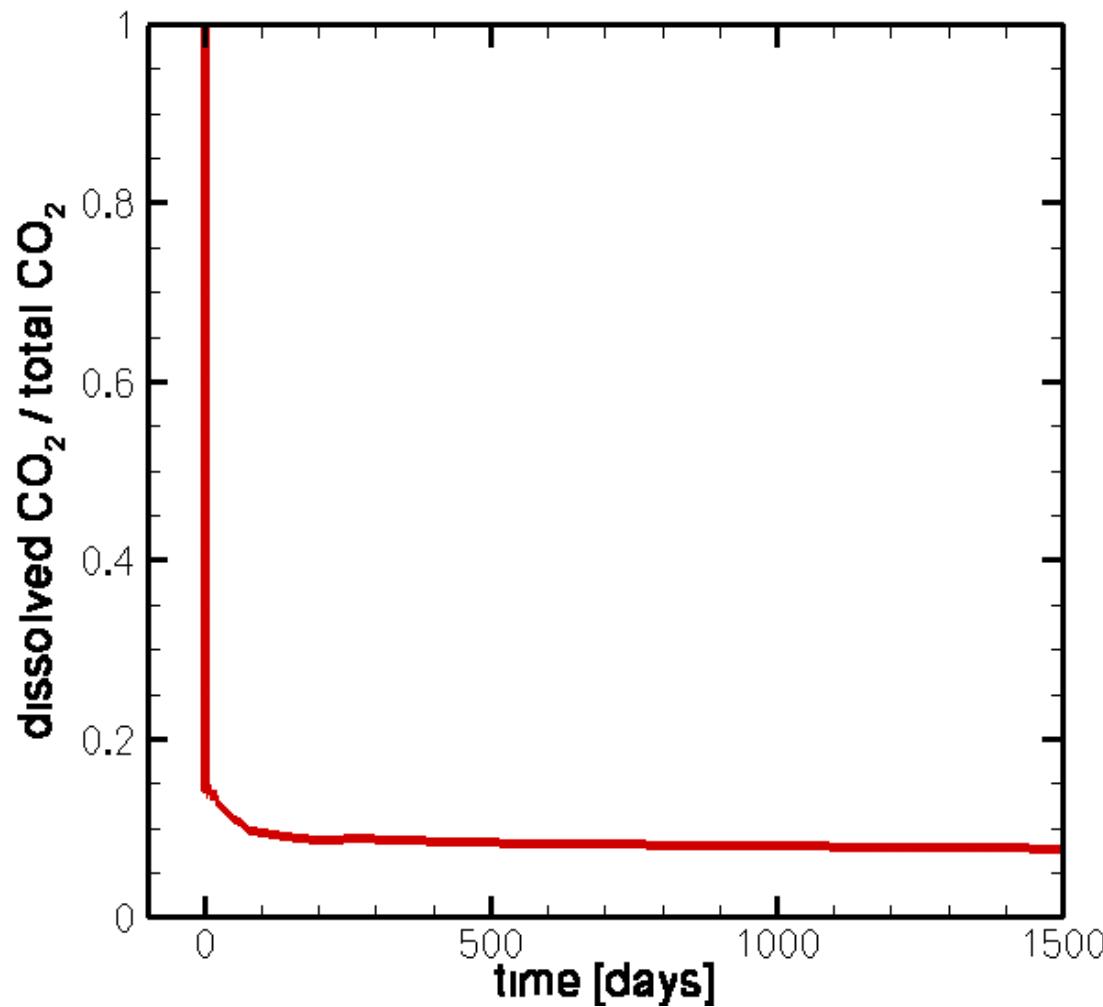
Simulation(2): Results

Mass of injected CO₂ in domain

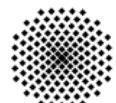
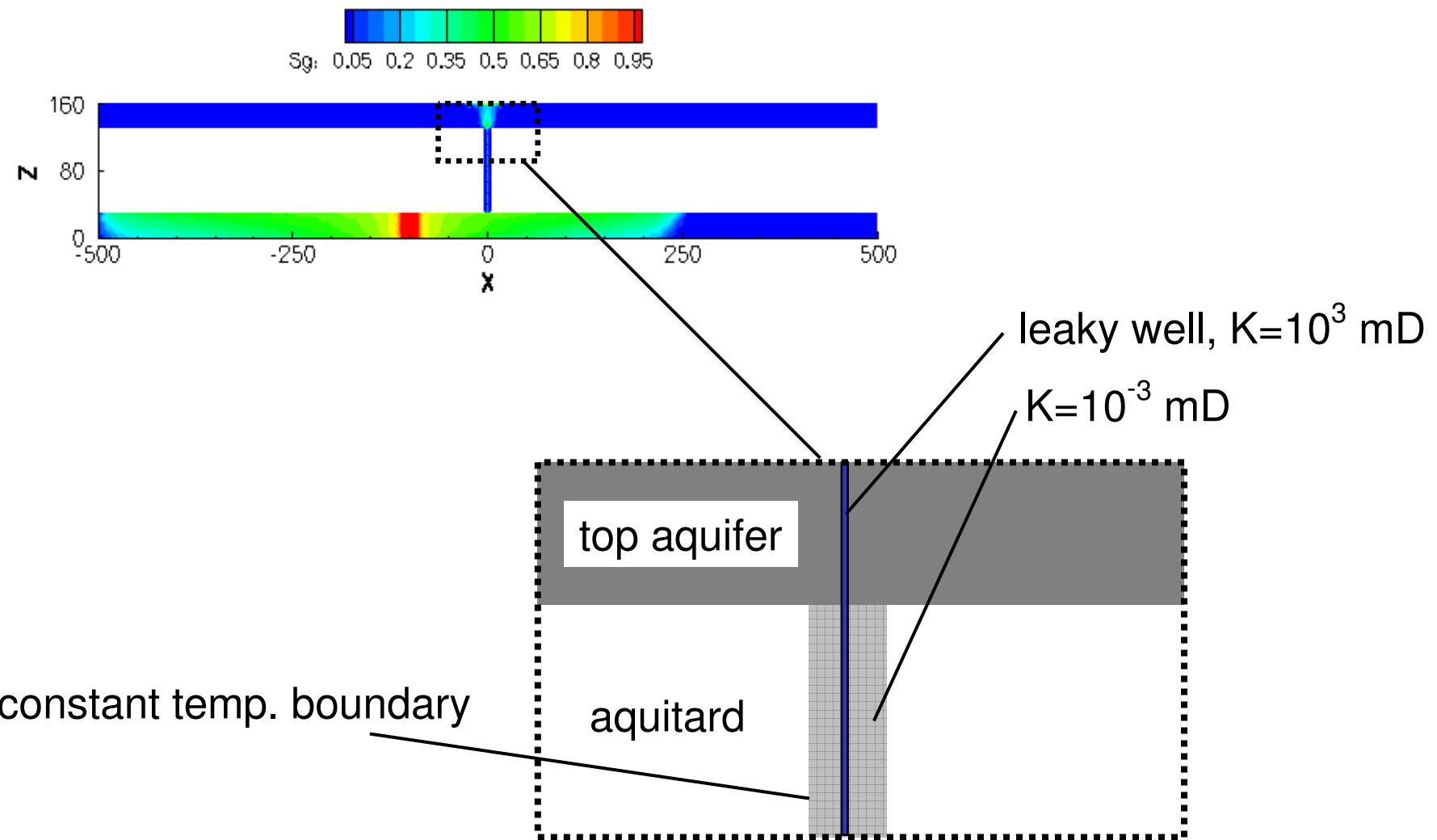


Simulation(2): Results

Fraction of the total mass of CO₂ dissolved in brine

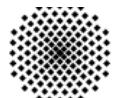
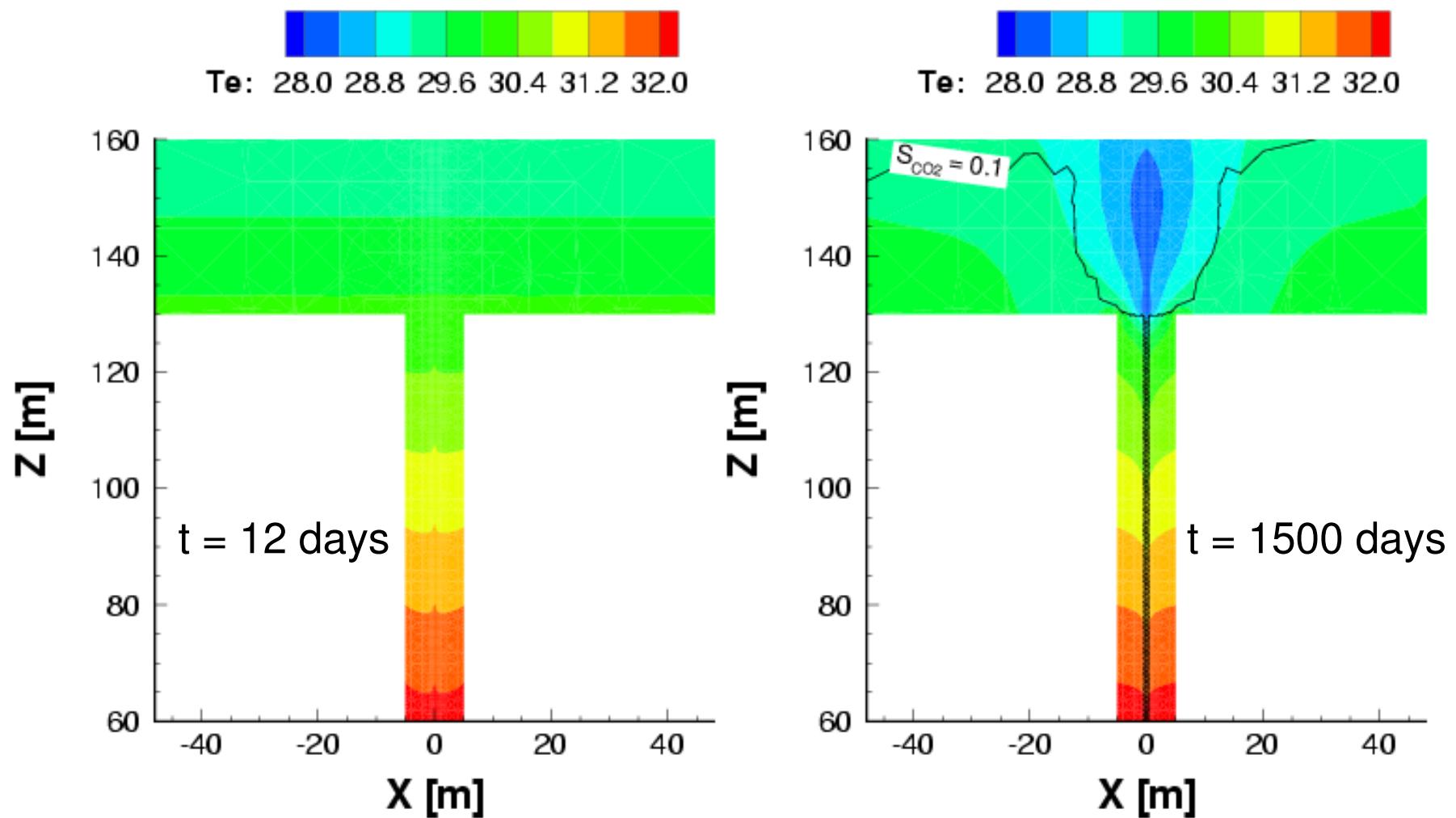


Simulation(2): Results



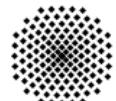
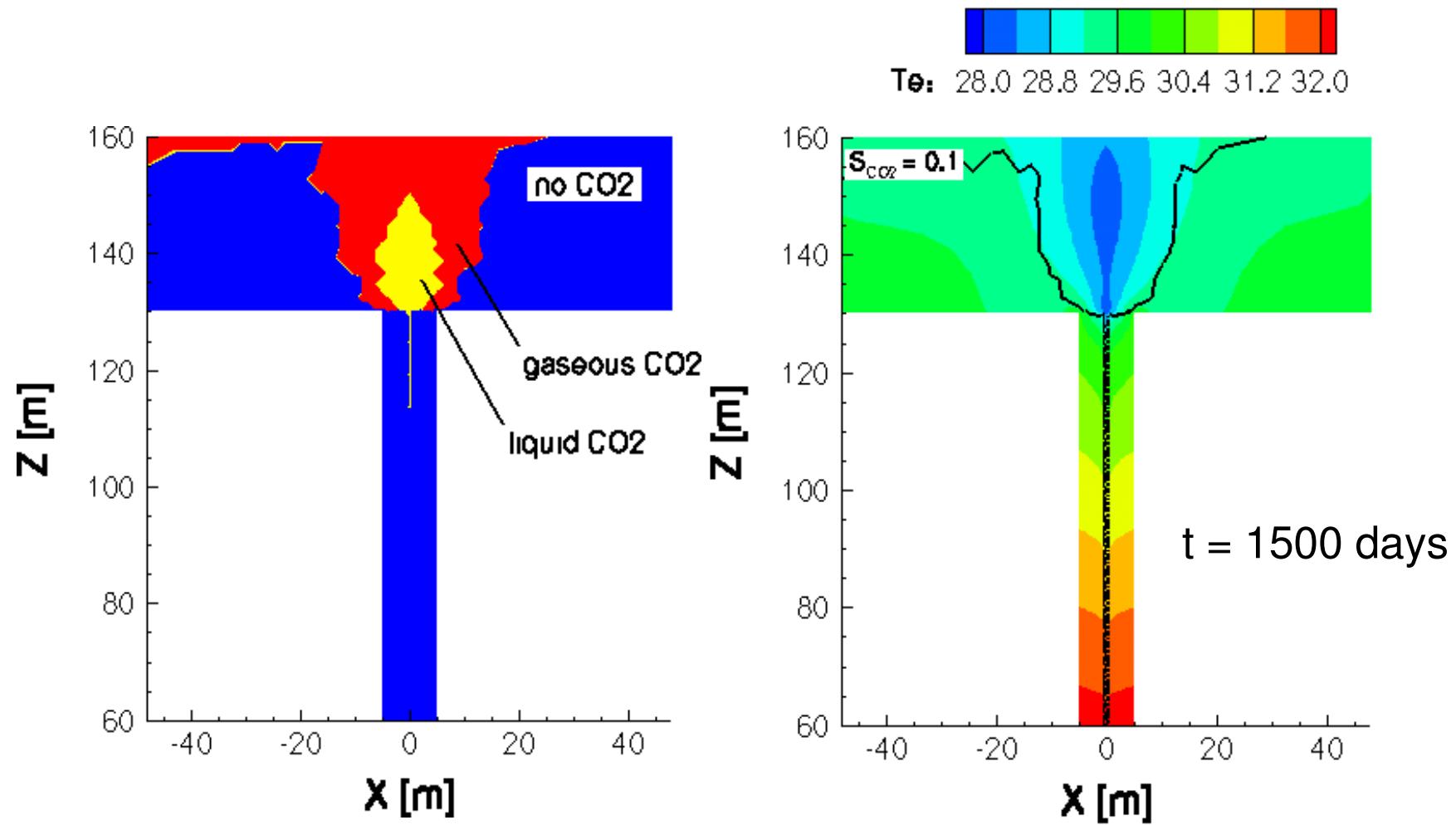
Simulation(2): Results

Temperature [°C] at the top of the leaky well



Simulation(2): Results

Temperature [°C] at the top of the leaky well and state of CO₂



Summary & Outlook

Reliability of a numerical model for CO₂ injection and storage in deep geological formations depends on

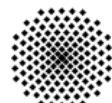
- Validity of the simplifying assumptions (are the governing processes sufficiently reproduced?)
- Accuracy of the mathematical and numerical model

Gaining confidence in the model requires a validation/verification

- Possible for simple problems by comparison with (semi-)analytical solutions
- Hardly feasible for complex problems due to a lack of well-controlled experimental or field data

Strategy for improving the confidence in complex models

- Application of the models for the simulation of field-scale projects, e.g. Ketzin (CO2SINK) with detailed monitoring and measurement campaigns.
- Code intercomparison with benchmark problems



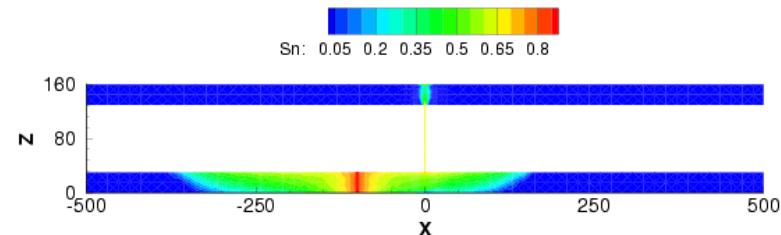
International Workshop on CO₂-Modelling

Numerical Models for CO₂ Storage in Geological Formations

Aims:

- presenting the current capabilities of mathematical and numerical models for CO₂ storage in geological formations
- discussing the future developments and application of numerical models for large-scale CO₂ storage projects
- model intercomparison study: benchmarks will be announced by August 2007

www.iws.uni-stuttgart.de/co2-workshop



Organizing Committee:

A. Ebigbo, H. Class, R. Helmig, A. Kopp

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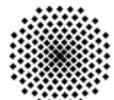
H. Dahle, J. Nordbotten

University of Bergen (Norway)

Mike Celia

Princeton University (USA)

Stuttgart, April 2.- 4., 2008



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